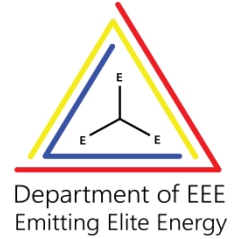




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Analog Electronic Circuits -BEE303

Module-II: Multistage Amplifiers & Feedback amplifiers:

Module II

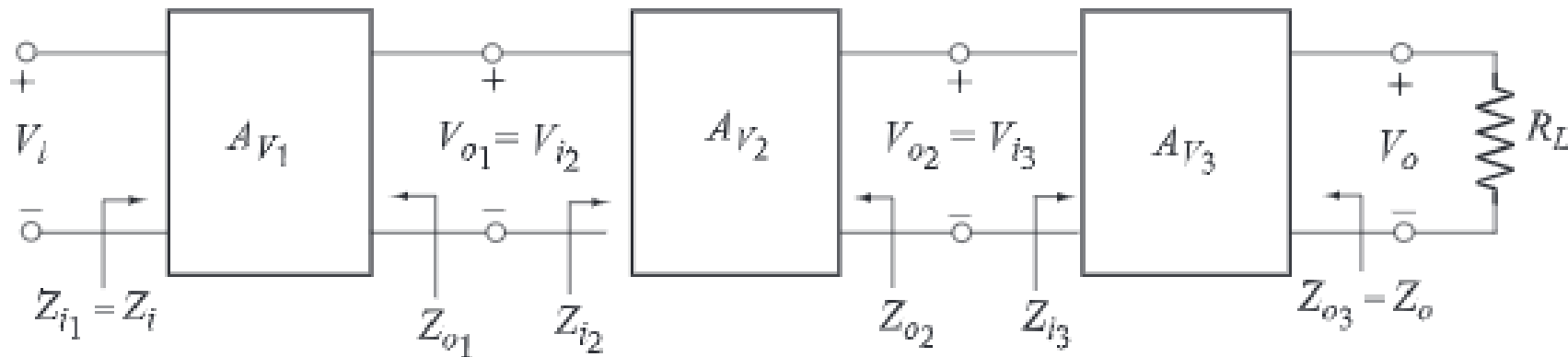
- **Multistage amplifiers:** Cascade and cascode connections, Darlington circuits, analysis and design.
- **Feedback amplifiers:** Feedback concept, different types, practical feedback circuits, analysis and design of feedback circuits.

In cascading, the output of one amplifier is connected to the input of another amplifier. It is used to increase gain while obtaining desired values of input and output resistances. Overall input resistance is the same as input resistance of the first amplifier and net output resistance is the same as output resistance of the last (n^{th}) amplifier in the network. When amplifiers are connected in cascade, then loading effect does occur.

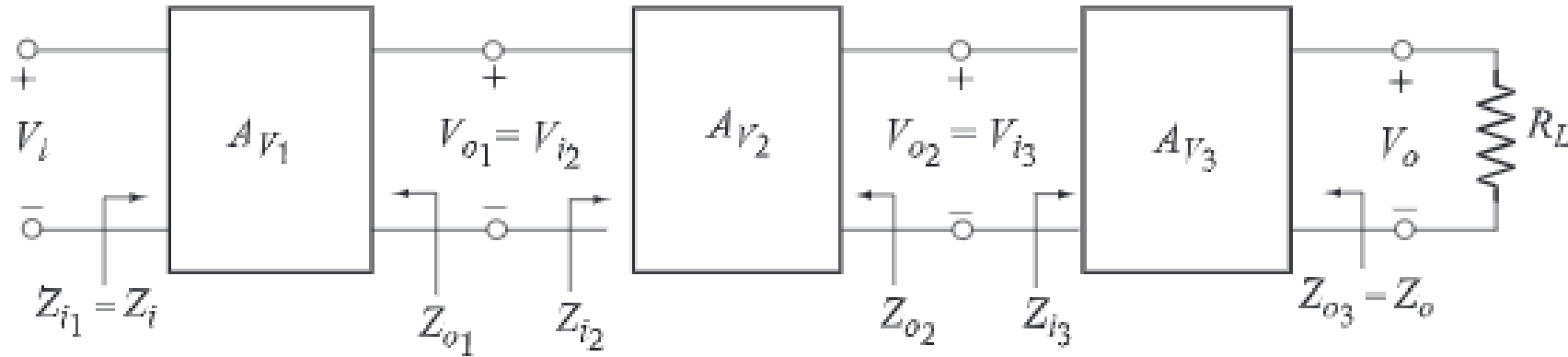
Multistage Amplifiers: Cascade Connection

When the amplification from a single stage amplifier is not **sufficient for a particular purpose** or when the input or output impedance is not of suitable magnitude for the intended application, **two or more stages are connected in series**.

The output of one stage is connected as input to the other stage.



Multistage Amplifiers: Cascade Connection



For the cascaded system, the input impedance is that of first stage and output impedance is that of last stage.

$$Z_i = Z_{i1} \quad \text{and} \quad Z_o = Z_{o3}$$

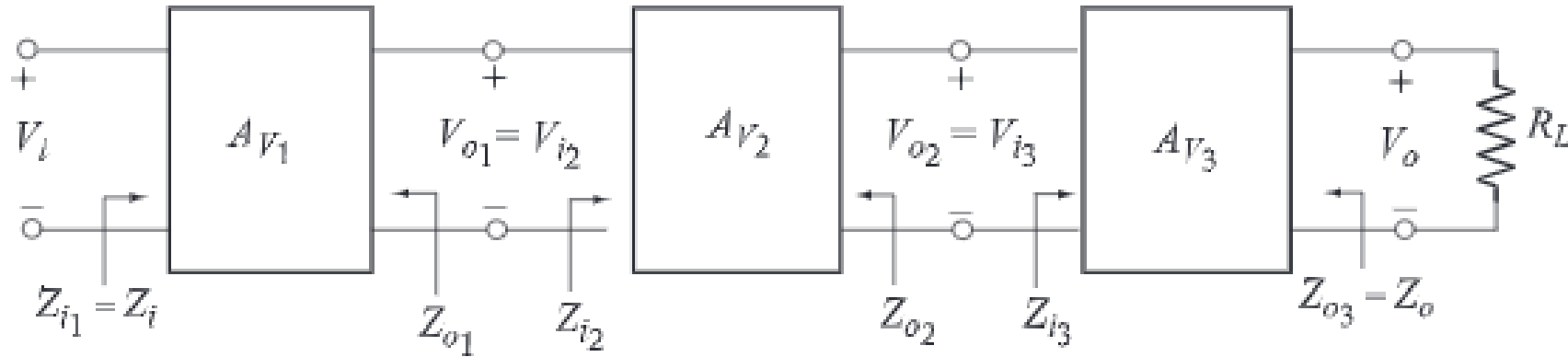
The output of one stage is connected as input to the other stage.

$$V_{i2} = V_{o1} \quad \text{and} \quad V_{i3} = V_{o2}$$

A total overall voltage gain of the cascading amplifier is:

$$A_{VT} = \frac{V_o}{V_i}$$

Multistage Amplifiers: Cascade Connection



A total overall voltage gain of the cascading amplifier is:

$$A_{VT} = \frac{V_o}{V_i}$$

$$A_{VT} = \frac{V_o}{V_{i3}} * \frac{V_{i3}}{V_{i2}} * \frac{V_{i2}}{V_i}$$

$$V_{i2} = V_{o1} \quad \text{and} \quad V_{i3} = V_{o2}$$

$$A_{VT} = \frac{V_o}{V_{i3}} * \frac{V_{o2}}{V_{i2}} * \frac{V_{o1}}{V_i}$$

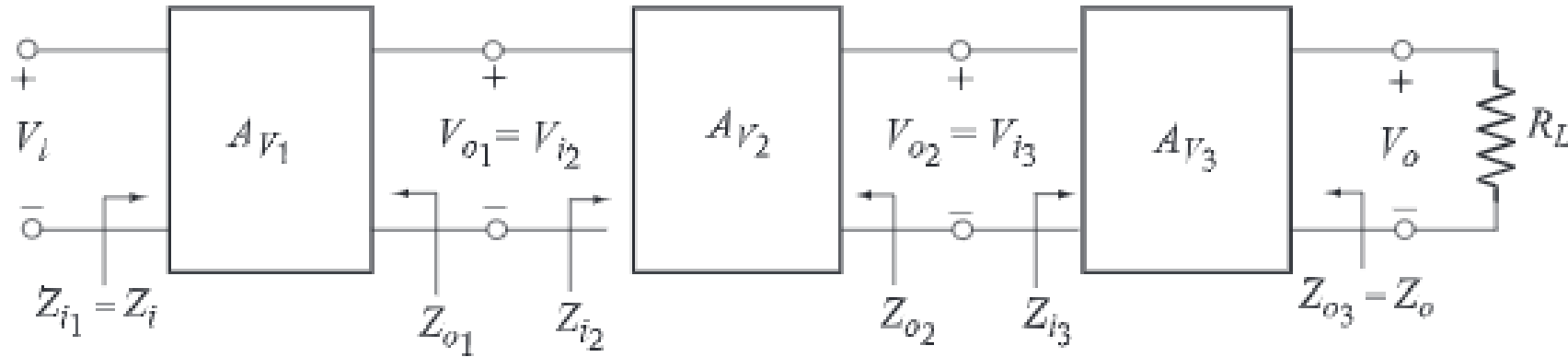
$$A_{VT} = A_{V3} * A_{V2} * A_{V1}$$

$$A_{VT} = A_{V1} * A_{V2} * A_{V3}$$

For n-cascaded amplifier stages,

$$A_{VT} = A_{V1} * A_{V2} * A_{V3} \text{ ----- } A_{Vn}$$

Multistage Amplifiers: Cascade Connection



A total overall current of the cascading amplifier is:

$$A_{IT} = -AVT * \frac{Z_{i1}}{R_L}$$

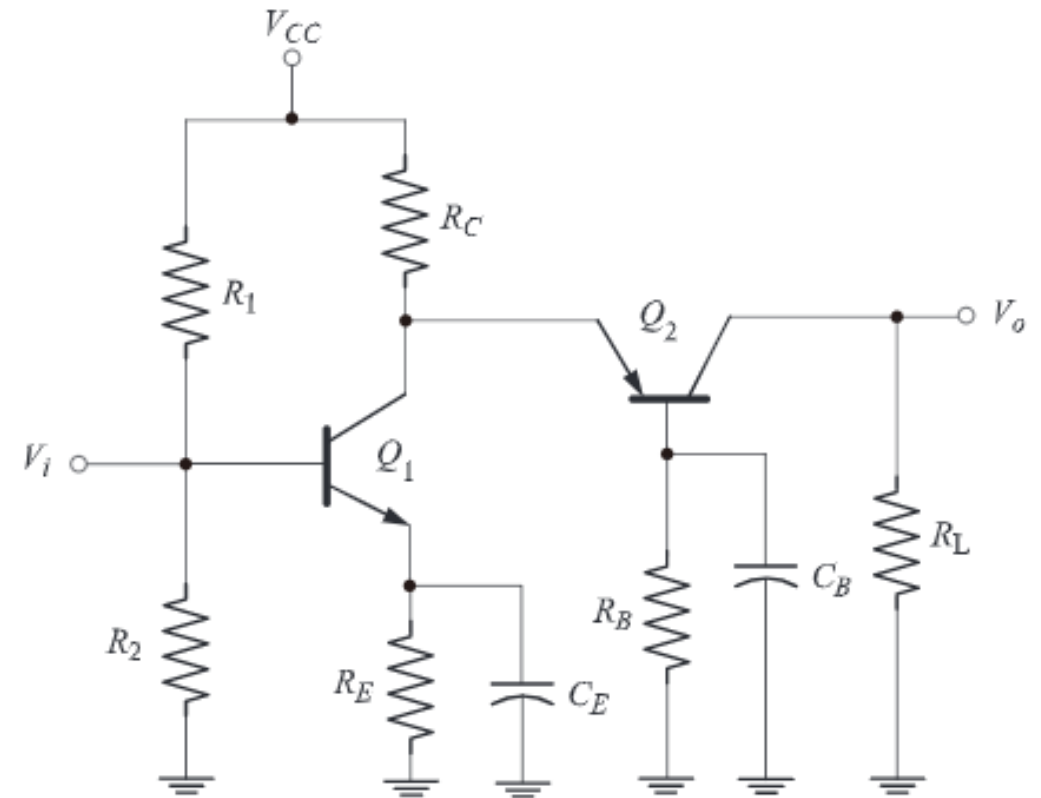
Multistage Amplifiers: Cascode Connection

In this connection the output of **Common Emitter (CE) stage drives the input of Common Base (CB) stage.**

1. Low input capacitance
2. High input impedance (provided by CE)
3. High output impedance (provided by CB)
4. Excellent high frequency response

The voltage gain of CE stage is very low.

R_B is used to limit the bias current of Q_2 .



Cascade Connection: Solved Examples

1. For the cascaded arrangement shown below, determine

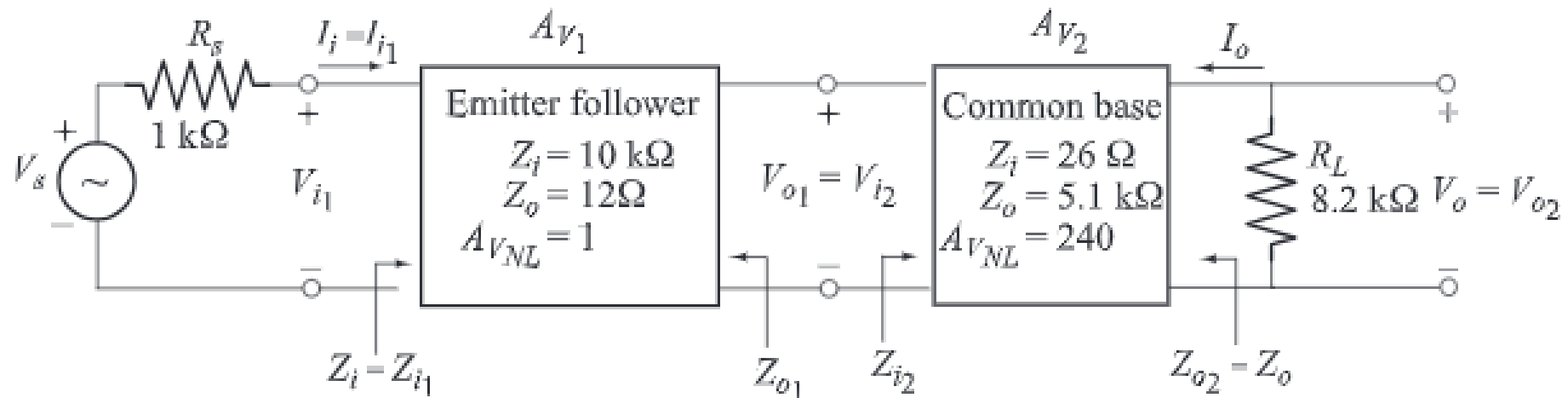
- The loaded voltage gain of each stage
- The total gain of the system, A_V and A_{VS}
- The total current gain of the system

Given:

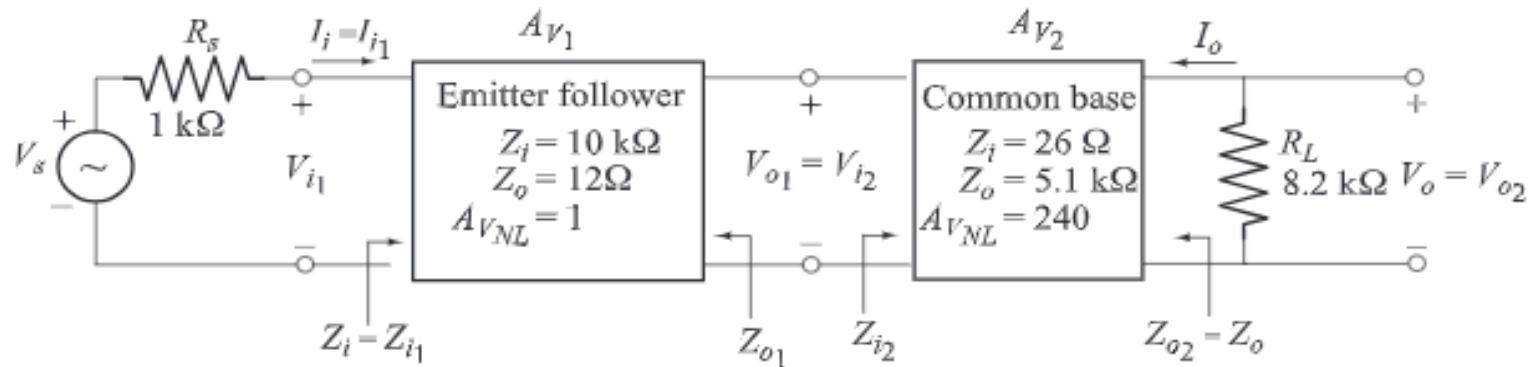
Stage 1: $Z_i = 10\text{k}\Omega$, $Z_o = 12\Omega$, $A_{VNL} = 1$

Stage 2: $Z_i = 26\Omega$, $Z_o = 5.1\text{k}\Omega$, $A_{VNL} = 240$

$R_S = 1\text{k}\Omega$, $R_L = 8.2\text{k}\Omega$



Cascade Connection: Solved Examples



a. The loaded gain of each stage

For the emitter follower stage the load is Z_{i2} .

$$A_{V1} = \frac{V_{o1}}{V_{i1}} = \frac{Z_{i2}}{Z_{i2} + Z_{o1}} A_{VNL}$$

$$A_{V1} = \frac{26}{26 + 12} * 1 = \mathbf{0.684}$$

$$A_{V2} = \frac{V_{o2}}{V_{i2}} = \frac{R_L}{R_L + Z_{o2}} A_{VNL}$$

$$A_{V2} = \frac{8.2k}{8.2k + 5.1k} * 240 = \mathbf{147.97}$$

b. Total voltage gain

$$A_{VT} = A_{V1} * A_{V2}$$

$$A_{VT} = 0.684 * 147.97 = \mathbf{101.20}$$

Cascade Connection: Solved Examples

$$A_{VS} = \frac{Z_{i1}}{Z_{i1} + R_S} A_{VT}$$

$$A_{VS} = \frac{10k}{10k + 1k} * 101.20 = \mathbf{92}$$

$$A_{VS} = \frac{Z_{i1}}{Z_{i1} + R_S} A_{VT}$$

$$A_{VS} = \frac{10k}{10k + 1k} * 101.20 = \mathbf{92}$$

c. Total current gain

$$A_{IT} = -A_{VT} * \frac{Z_{i1}}{R_L}$$

$$A_{IT} = -(101.20) * \frac{10k}{8.2k} = \mathbf{-123.41}$$

Cascade Connection: Solved Examples

1. For the cascaded arrangement shown below, determine

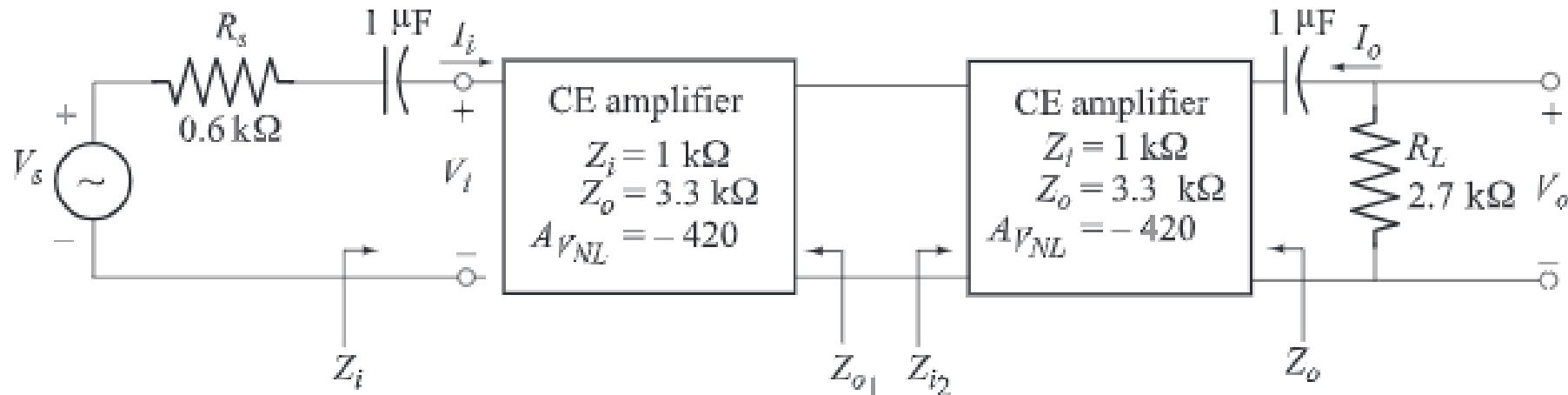
- The loaded voltage gain of each stage
- The total gain of the system, A_V and A_{VS}
- The current gain of each stage
- The total current gain

Given:

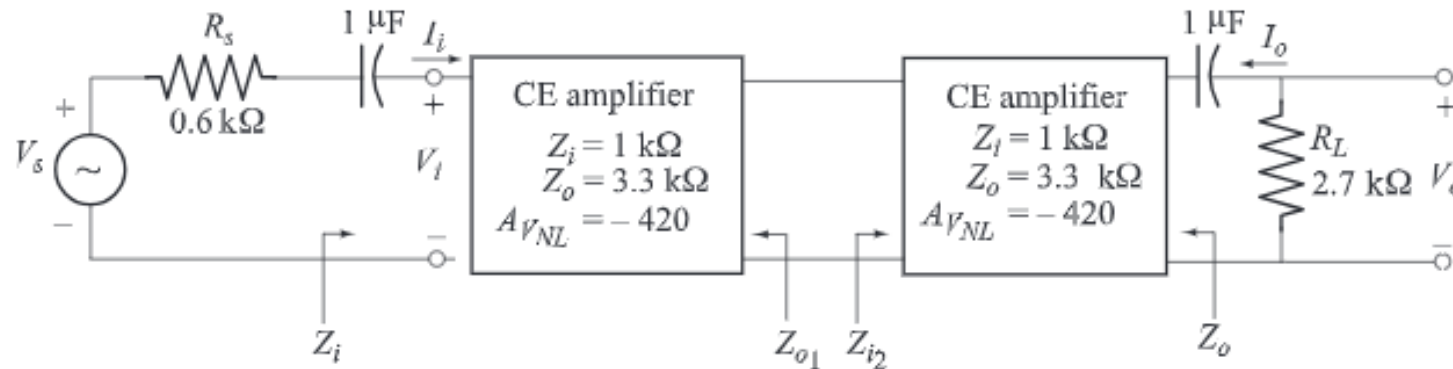
Stage 1: $Z_i = 1\text{k}\Omega$, $Z_o = 3.3\text{k}\Omega$, $A_{VNL} = -420$

Stage 2: $Z_i = 1\text{k}\Omega$, $Z_o = 3.3\text{k}\Omega$, $A_{VNL} = -420$

$R_S = 0.6\text{k}\Omega$, $R_L = 2.7\text{k}\Omega$



Cascade Connection: Solved Examples



a. The loaded gain of each stage

The Load on the 1st stage the load is Z_{i2} .

$$A_{V1} = \frac{V_{o1}}{V_{i1}} = \frac{Z_{i2}}{Z_{i2} + Z_{o1}} A_{VNL}$$

$$A_{V1} = \frac{1k}{1k + 3.3k} * -420 = -\mathbf{97.67}$$

$$A_{V2} = \frac{V_{o2}}{V_{i2}} = \frac{R_L}{R_L + Z_{o2}} A_{VNL}$$

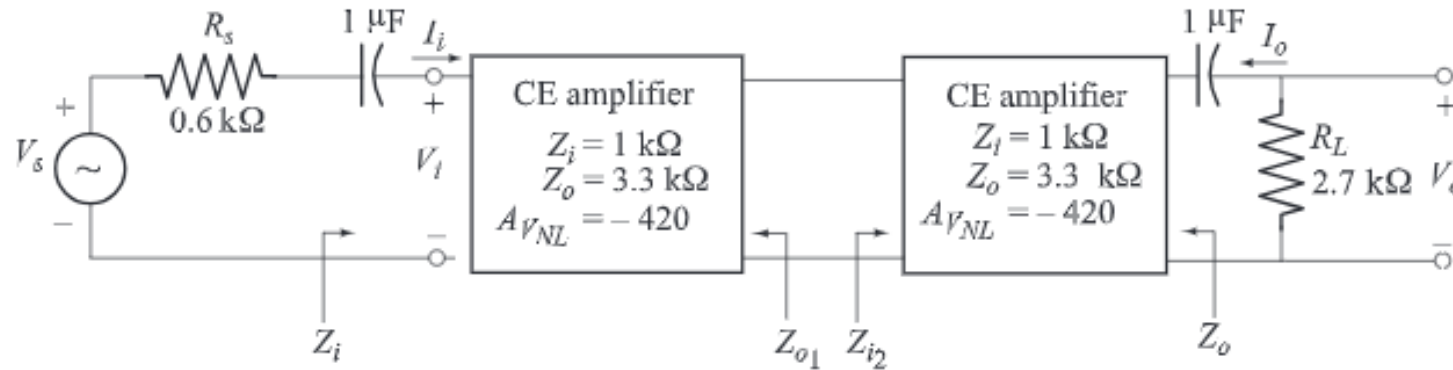
$$A_{V2} = \frac{2.7k}{2.7k + 3.3k} * -420 = -\mathbf{189}$$

b. Total voltage gain

$$A_{VT} = A_{V1} * A_{V2}$$

$$A_{VT} = -97.67 * -189 = \mathbf{18.45 * 103}$$

Cascade Connection: Solved Examples



$$A_{VS} = \frac{Z_{i1}}{Z_{i1} + R_S} A_{VT}$$

$$A_{VS} = \frac{1k}{1k + 0.6k} * 18.45 * 10^3 = \mathbf{11.53 * 10^3}$$

c. Current gain of each stage

$$A_{I1} = -A_{V1} * \frac{Z_{i1}}{Z_{i2}}$$

$$A_{I1} = -(-97.67) * \frac{1k}{1k} = \mathbf{97.67}$$

$$A_{I2} = -A_{V2} * \frac{Z_{i2}}{R_L} = -(-189) * \frac{1k}{2.7k} = \mathbf{70}$$

$$A_{iT} = A_{i1} * A_{i2} = 97.67 * 70 = \mathbf{6.84 * 10^3}$$

Darlington Amplifier

β_1 = Current gain of Q_1

β_2 = Current gain of Q_2

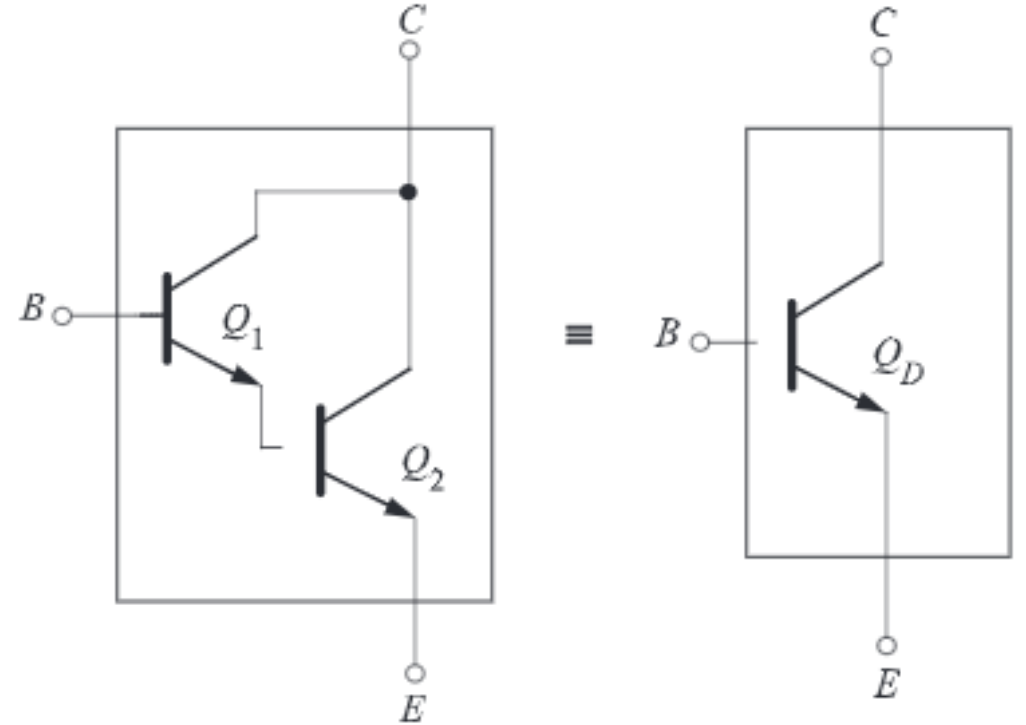
The current gain of Darlington Transistor:

$$\beta_D = \beta_1 * \beta_2$$

If $\beta_1 = \beta_2 = \beta$

$$\beta_D = \beta^2$$

A Darlington connection acts as single transistor with a **large current gain**.



Darlington Amplifier: DC Bias

Applying KVL to the Base-Emitter circuit we get;

$$V_{CC} - I_B R_B - V_{BE} - I_E R_E = 0$$

$$V_{BE} = V_{BE1} + V_{BE2}$$

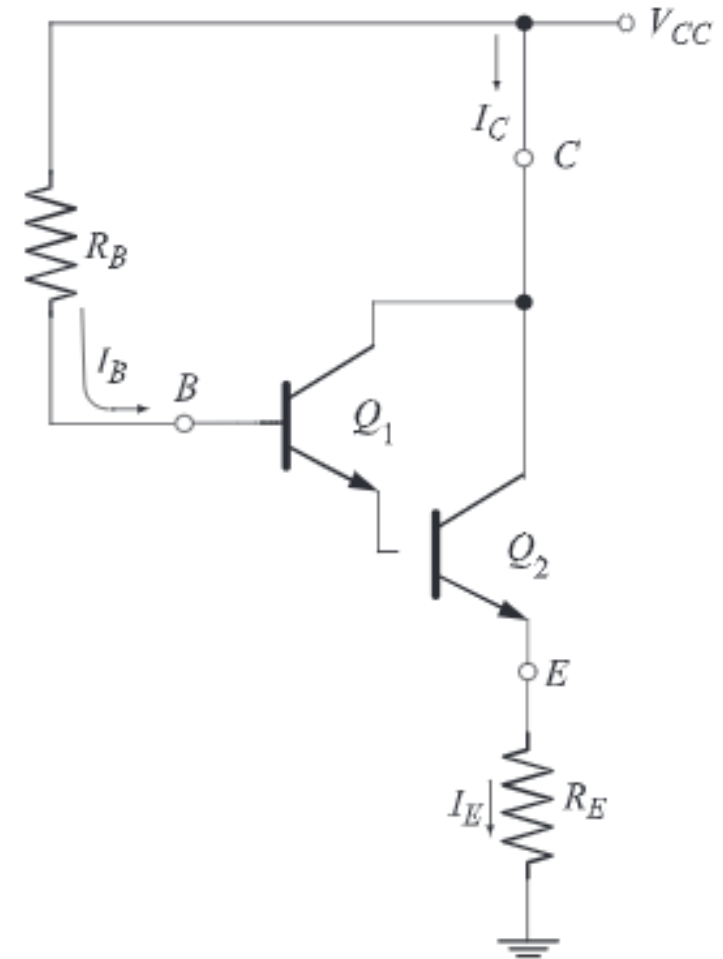
$$I_E = (1 + \beta_D) I_B \approx \beta_D I_B$$

$$I_B R_B = V_{CC} - V_{BE} - I_E R_E$$

$$I_B = \frac{V_{CC} - V_{BE}}{R_B + (1 + \beta_D) R_E}$$

$$V_E = I_E * R_E$$

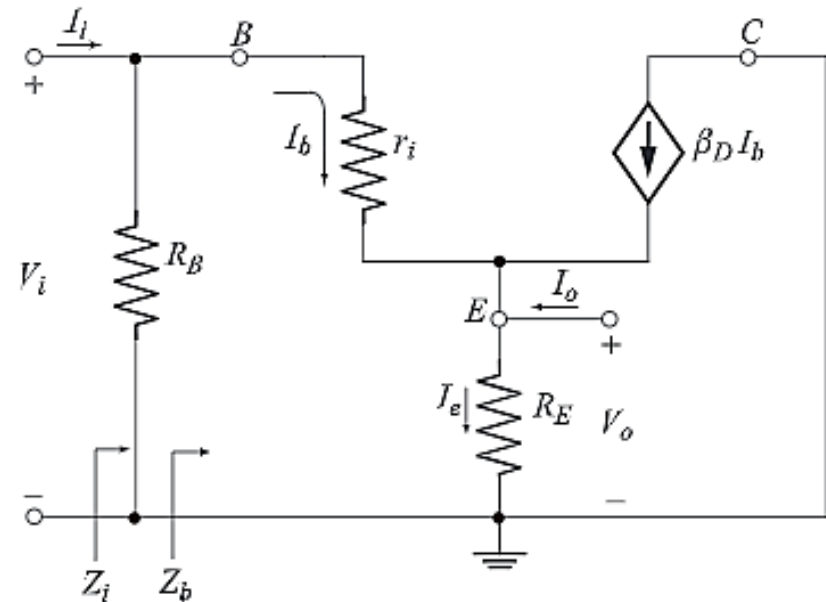
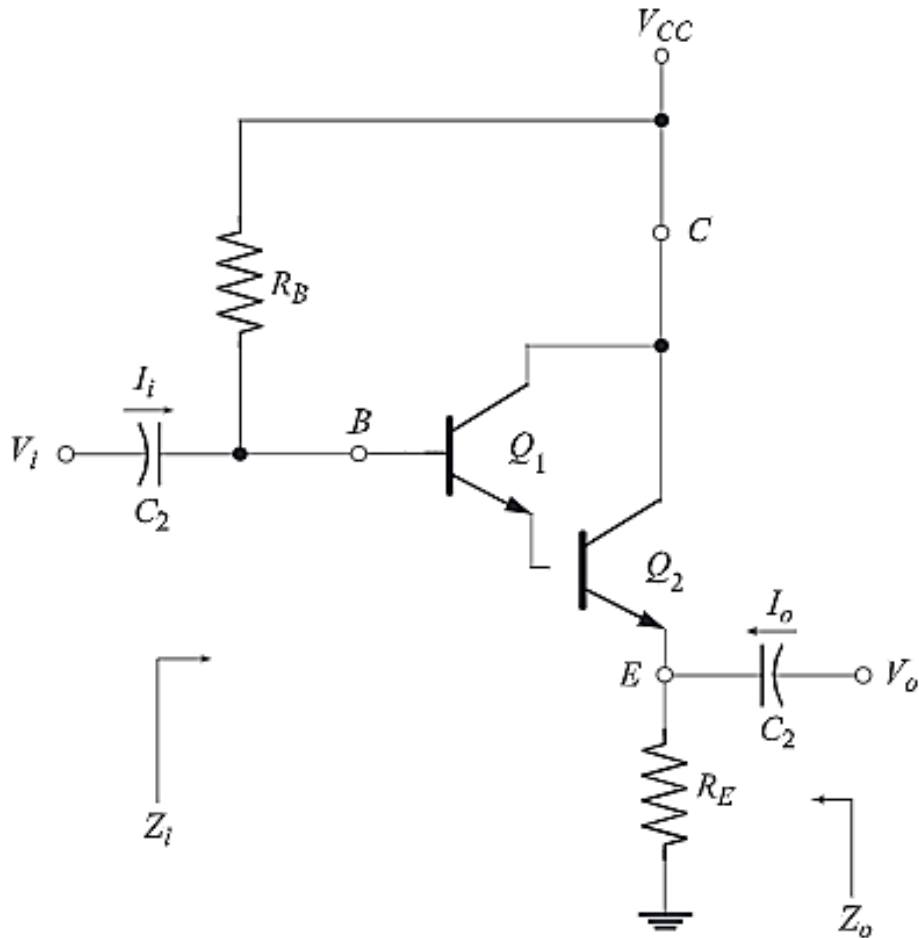
$$V_B = V_{BE} + V_E$$



Darlington Emitter Follower

The Darlington transistor is replaced by

- 1. Input resistance r_i between base and emitter.**
- 2. Controlled current source between collector and emitter terminals.**



AC equivalent circuit of Darlington transistor

Darlington Emitter Follower

AC Input Impedance (Z_I):

Applying KVL to the circuit we get;

$$V_I = I_b r_i + I_e R_E$$

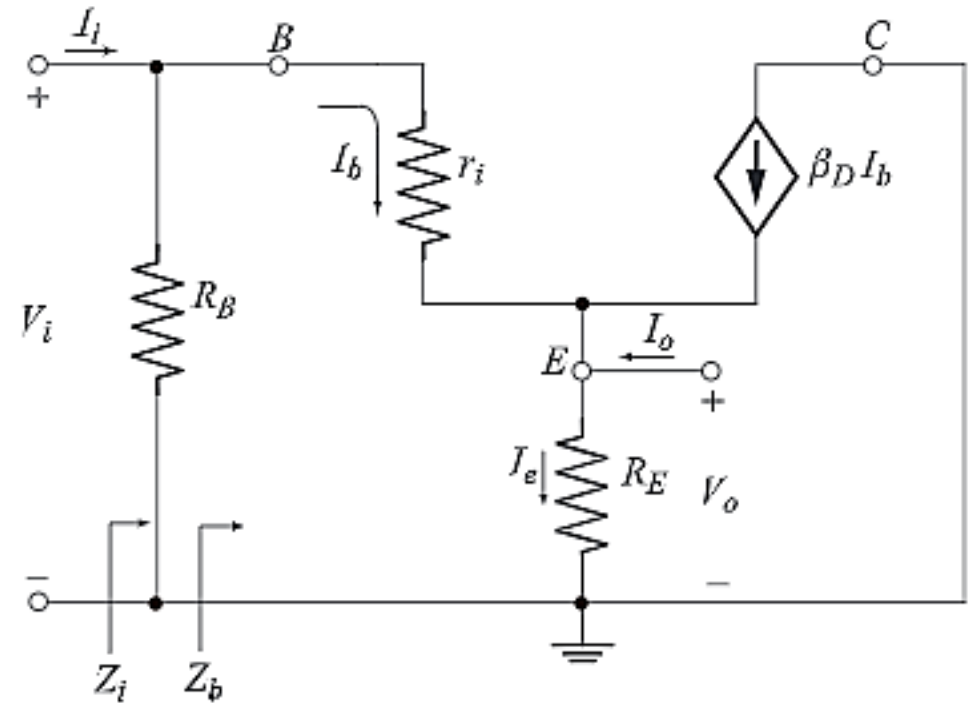
$$I_e = (1 + \beta_D) I_b$$

$$V_I = I_b r_i + (1 + \beta_D) I_b R_E$$

$$Z_b = \frac{V_I}{I_b} = r_i + (1 + \beta_D) R_E \approx \beta_D R_E$$

Since β_D is Very High

$$Z_I = \frac{V_I}{I_I} = R_B \parallel Z_b$$



AC equivalent circuit

Darlington Emitter Follower

AC Current Gain (A_I):

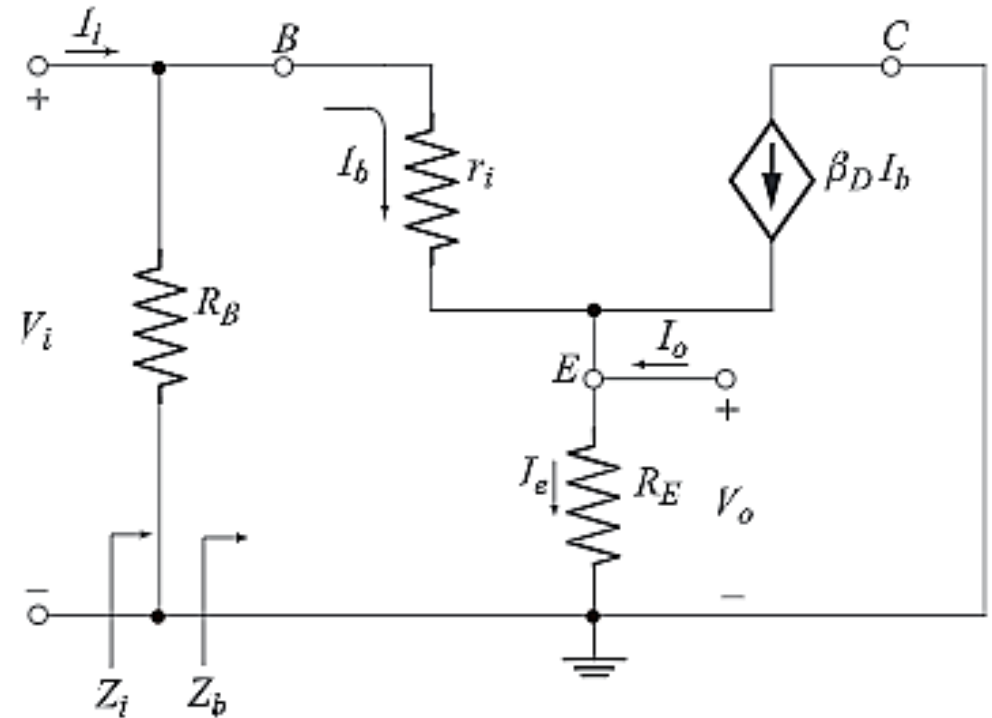
$$A_I = \frac{I_O}{I_I} = \frac{I_O}{I_b} * \frac{I_b}{I_I}$$

$$I_O = I_e$$

$$A_I = \frac{I_e}{I_I} = \frac{I_e}{I_b} * \frac{I_b}{I_I}$$

$$I_e = (1 + \beta_D) I_b \approx \beta_D I_b$$

$$\frac{I_e}{I_b} = \beta_D$$



AC equivalent circuit

Darlington Emitter Follower

AC Current Gain (A_I):

Applying KCL to the circuit we get;

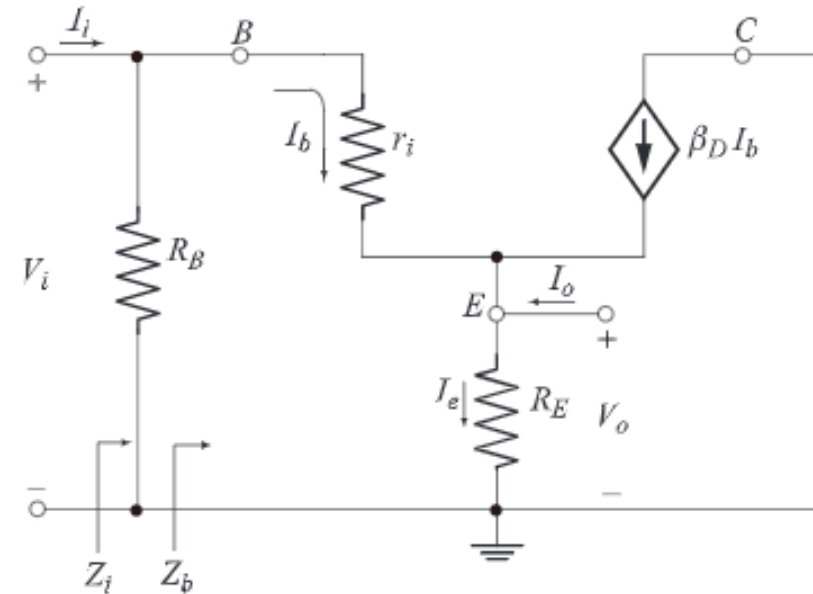
$$I_I = \frac{V_I}{R_B} + I_b$$

Using $V_i = I_b Z_b$ we get

$$I_I = \frac{I_b Z_b}{R_B} + I_b = \left[\frac{Z_b}{R_B} + 1 \right] * I_b$$

$$I_I = \left[\frac{Z_b + R_B}{R_B} \right] * I_b$$

$$\frac{I_b}{I_I} = \frac{R_B}{Z_b + R_B}$$



AC equivalent circuit

$$A_I = \frac{\beta_D R_B}{Z_b + R_B} = \frac{\beta_D R_B}{\beta_D R_E + R_B}$$

Darlington Emitter Follower

AC Voltage Gain (A_V):

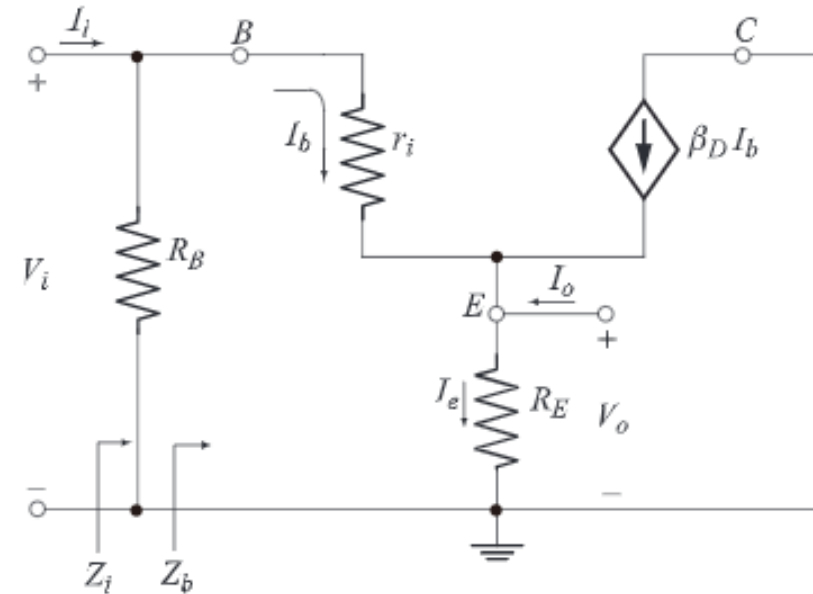
$$V_O = I_e R_E$$

$$V_O = (1 + \beta_D) I_b R_E$$

$$V_I = I_b [r_i + (1 + \beta_D) R_E]$$

$$A_V = \frac{V_O}{V_I} = \frac{(1 + \beta_D) I_b R_E}{I_b [r_i + (1 + \beta_D) R_E]}$$

$$A_V = \frac{V_O}{V_I} = \frac{(1 + \beta_D) R_E}{[r_i + (1 + \beta_D) R_E]} \approx 1$$



AC equivalent circuit

Darlington Emitter Follower

AC Output Impedance (Z_O):

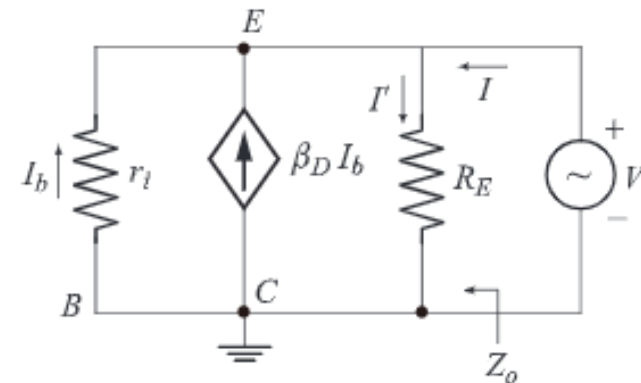
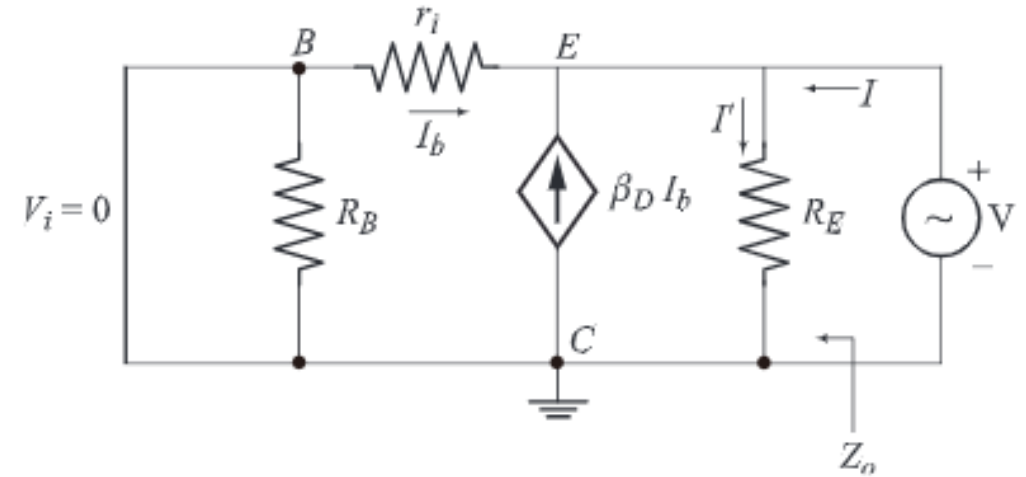
Applying KCL to the circuit we get;

$$I_b + \beta_D I_b - I^I + I = 0$$

$$I_b = \frac{-V}{r_i} \quad \text{and} \quad I^I = \frac{V}{R_E}$$

$$\frac{-V}{r_i} + \beta_D \frac{-V}{r_i} - \frac{V}{R_E} + I = 0$$

$$\left[\frac{1}{r_i} + \frac{\beta_D}{r_i} + \frac{1}{R_E} \right] V = I$$



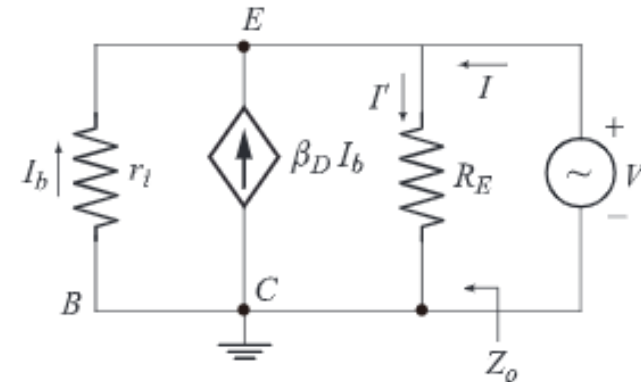
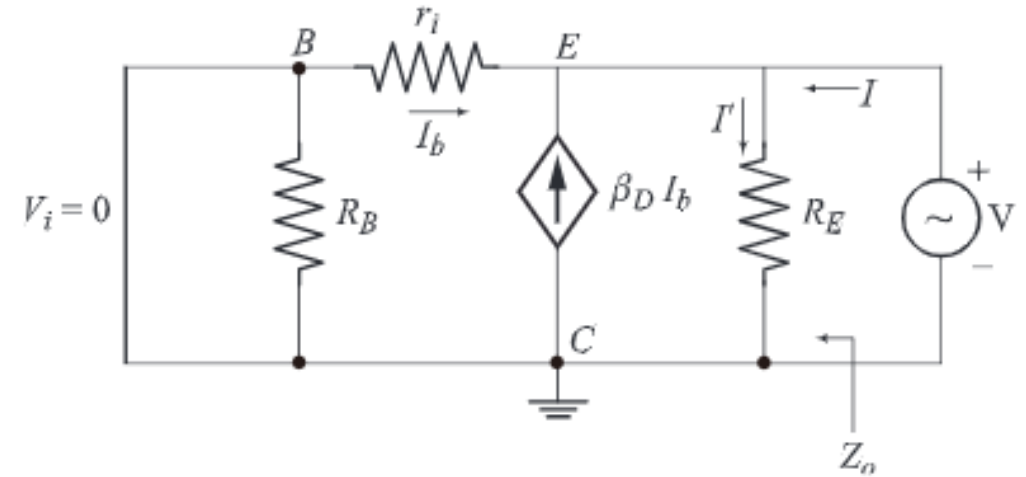
Darlington Emitter Follower

AC Output Impedance (Z_O):

$$Z_O = \frac{V}{I} = \frac{1}{\left[\frac{1}{r_i} + \frac{\beta_D}{r_i} + \frac{1}{R_E} \right]}$$

$$Z_O = \frac{V}{I} = \frac{1}{\left[\frac{1}{r_i} + \frac{1}{r_i/\beta_D} + \frac{1}{R_E} \right]}$$

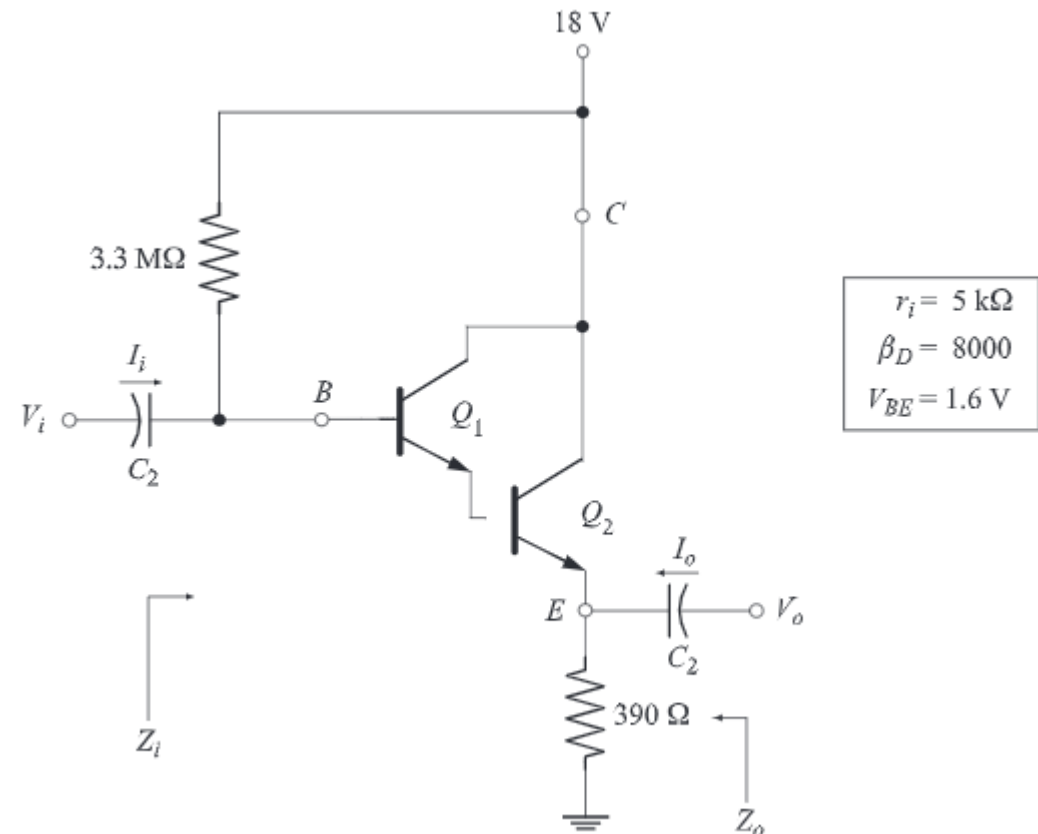
$$Z_O = \left[r_i \parallel R_E \parallel \frac{r_i}{\beta_D} \right] \approx \frac{r_i}{\beta_D}$$



Darlington Emitter Follower

For the Darlington emitter-follower shown below:

- (a) Calculate the dc bias voltages V_B , V_E , V_C and currents I_B and I_C .
- (b) Calculate the input and output impedances.
- (c) Determine the voltage and current gains.



Darlington Emitter Follower

(a)

$$\begin{aligned} I_B &= \frac{V_{CC} - V_{BE}}{R_B + \beta_D R_E} \\ &= \frac{18\text{ V} - 1.6\text{ V}}{3.3\text{ M}\Omega + (8000)(390\Omega)} = 2.55\text{ }\mu\text{A} \end{aligned}$$

$$\begin{aligned} I_E &= I_{E2} \approx I_{C2} = \beta_D I_B \\ &= (8000)(2.55\text{ }\mu\text{A}) = 20.4\text{ mA} \end{aligned}$$

$$V_E = I_E R_E = (20.4\text{ mA})(390\text{ }\Omega) = 7.96\text{ V}$$

$$V_B = V_{BE} + V_E = 1.6\text{ V} + 7.96\text{ V} = 9.56\text{ V}$$

Since the collector is directly tied to V_{CC} , the collector voltage equals the dc supply voltage V_{CC} .

$$\therefore V_C = V_{CC} = 18\text{ V}$$

Darlington Emitter Follower

(b)

$$Z_b = r_i + (1 + \beta_D) R_E$$

$$= 5 \text{ k}\Omega + (8001) (390 \text{ }\Omega) = 3.13 \text{ M}\Omega$$

$$Z_i = R_B \parallel Z_b = 3.3 \text{ M}\Omega \parallel 3.13 \text{ M}\Omega = 1.6 \text{ M}\Omega$$

$$Z_o = r_i \parallel R_E \parallel \frac{r_i}{\beta_D}$$

$$= 5 \text{ k}\Omega \parallel 390 \text{ }\Omega \parallel \frac{5 \text{ k}\Omega}{8000} = 0.625 \text{ }\Omega$$

Darlington Emitter Follower

(c)

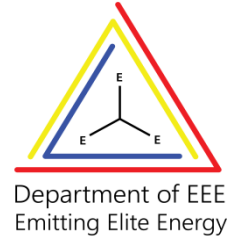
$$\begin{aligned} A_v &= \frac{R_E (1 + \beta_D)}{r_i + R_E (1 + \beta_D)} \\ &= \frac{(390\Omega)(8001)}{5\text{k}\Omega + (390\Omega)(8001)} = 0.998 \\ A_i &= \frac{\beta_D R_B}{R_B + \beta_D R_E} \\ &= \frac{(8000)(3.3\text{M}\Omega)}{3.3\text{M}\Omega + (8000)(390\Omega)} = 4112.15 \end{aligned}$$

(d)

$$\begin{aligned} V_o &= A_v V_i = (0.998)(120\text{ mV}) \\ &= 119.76\text{ mV} \end{aligned}$$



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Analog Electronic Circuits - 21EE32

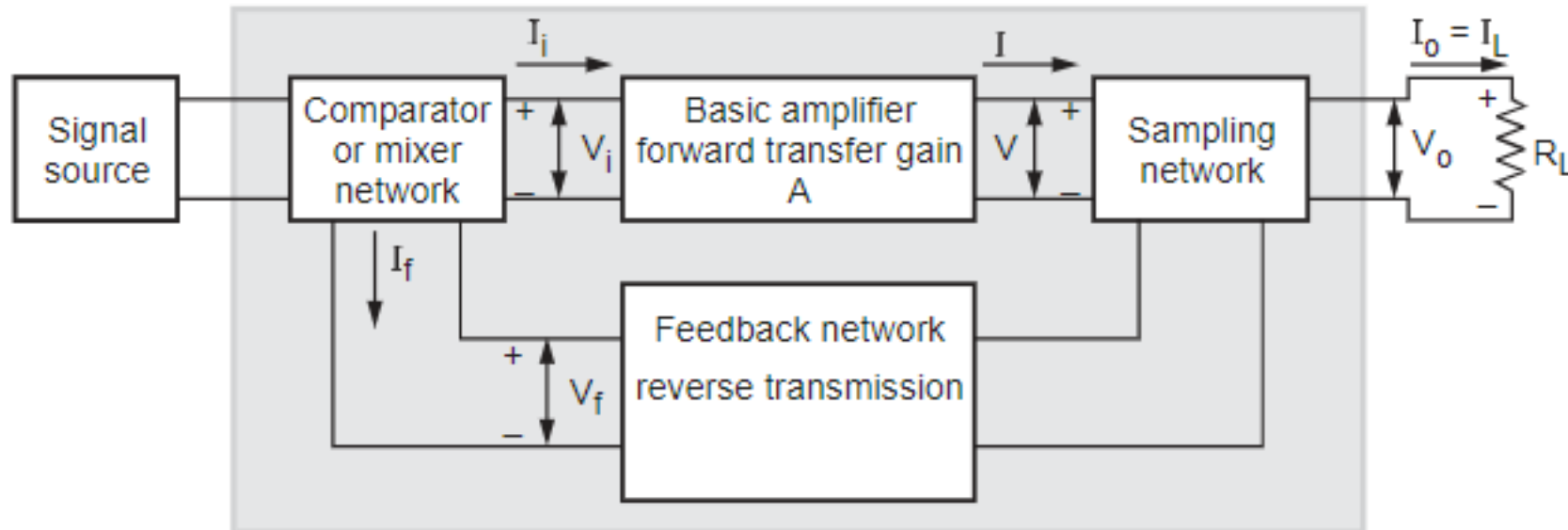
Module-II: Feedback Amplifiers

Feedback Amplifiers: Feedback concept, different types, practical feedback circuits, analysis and design of feedback circuits..

Feedback Amplifier

The amplifier in which a part of output is sampled & fed back to the input of the amplifier is called **feedback amplifier**.

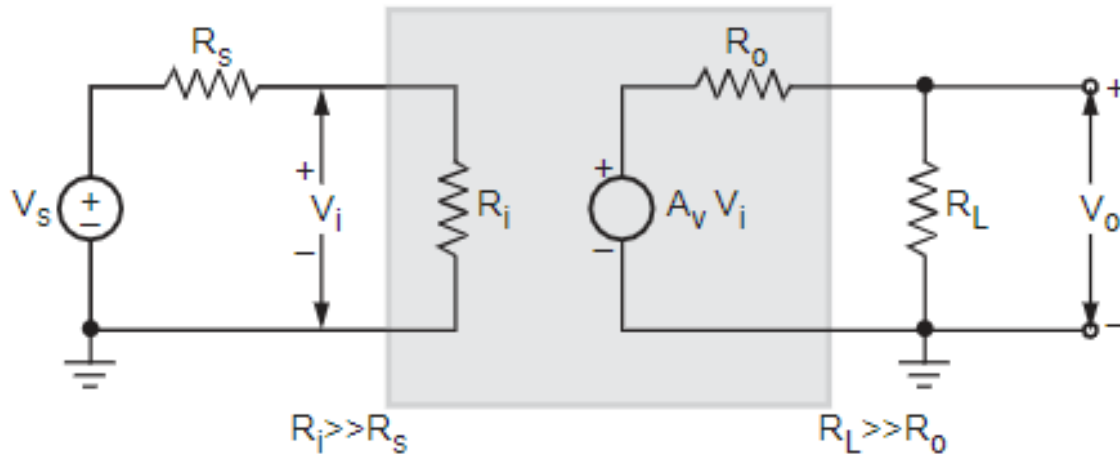
When input and a part of output signal are in phase, is called **positive feedback**. Used in Oscillators
When input and a part of signal are in out of phase, is called **negative feedback**. Used in Amplifiers



Use of Positive feedback results in oscillations and hence used in Oscillators and negative feedback gives stability and hence used in amplifiers

Feedback Amplifiers

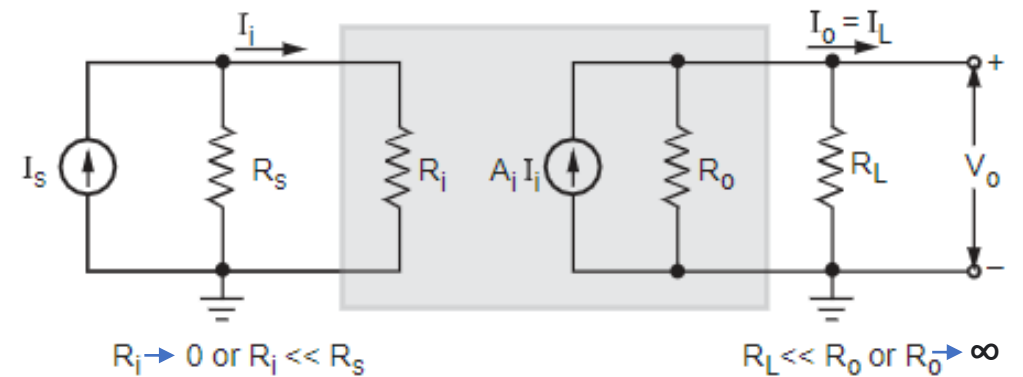
Voltage Amplifier



$$R_i \gg R_s \text{ and } R_L \gg R_o$$

For Ideal Case: $R_i = \text{Infinite}$ and $R_o = \text{Zero}$
Output voltage is proportional to the input voltage.

Current Amplifier

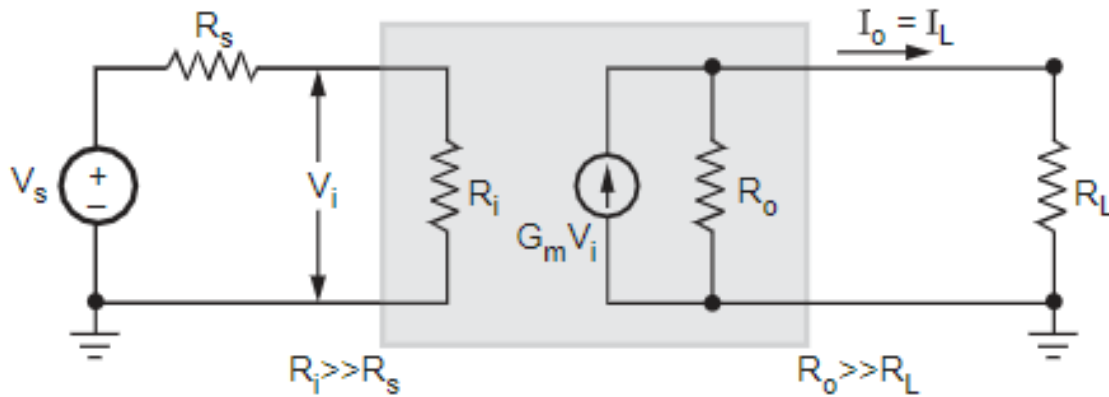


$$R_i \ll R_s \text{ and } R_L \ll R_o$$

For Ideal Case: $R_i = \text{Zero}$ and $R_o = \text{Infinite}$
Output current is proportional to input current.

Feedback Amplifiers

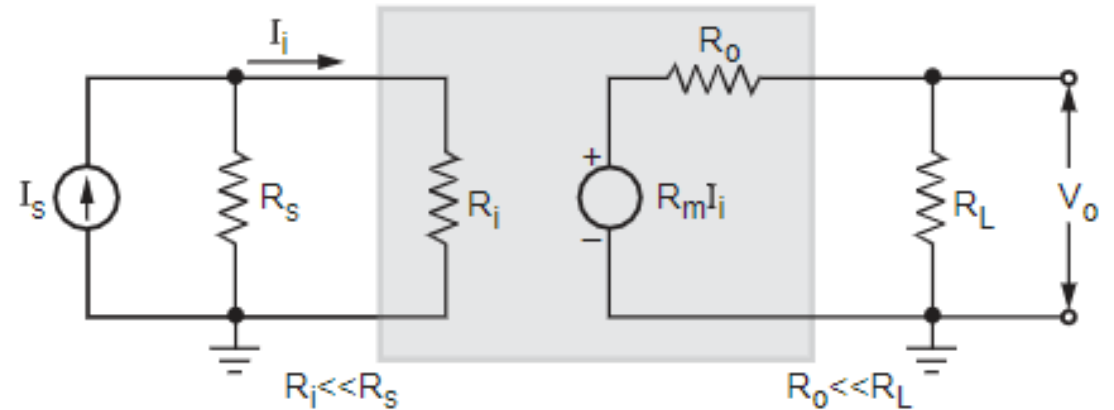
Transconductance Amplifier



$$R_i \gg R_s \text{ and } R_L \ll R_o$$

For Ideal Case: $R_i = \text{Infinite}$ and $R_o = \text{Infinite}$
Output current is proportional to the input voltage.

Transresistance Amplifier



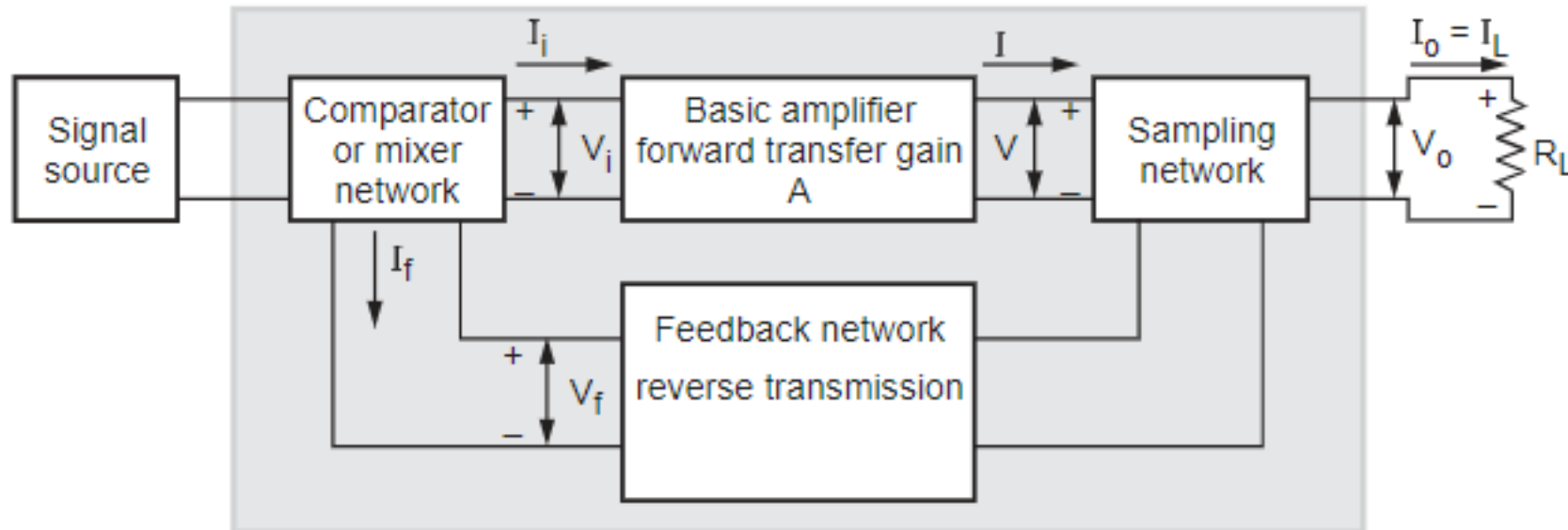
$$R_i \ll R_s \text{ and } R_o \ll R_L$$

For Ideal Case: $R_i = \text{Zero}$ and $R_o = \text{Zero}$
Output voltage is proportional to input current.

Feedback Amplifier

The amplifier in which a part of output is sampled & fed back to the input of the amplifier is called **feedback amplifier**.

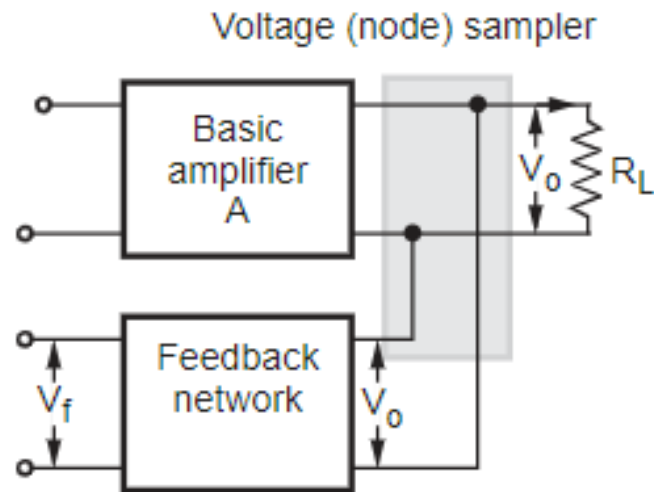
When input and a part of output signal are in phase, is called **positive feedback**. Used in Oscillators
When input and a part of signal are in out of phase, is called **negative feedback**. Used in Amplifiers



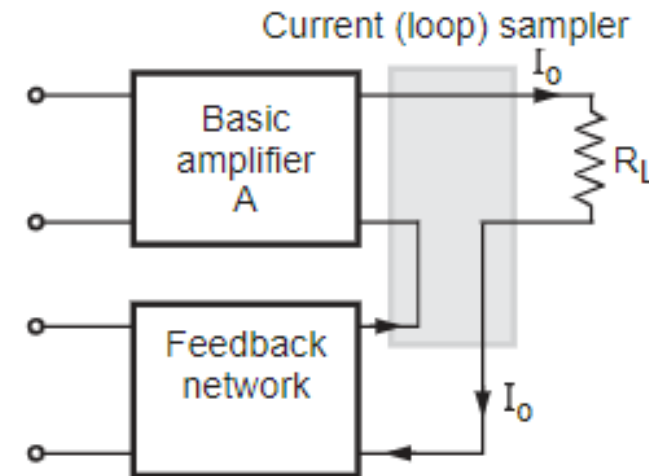
Feedback Structure

Sampling Network:

- The **output voltage** is sampled by connecting feedback network in shunt across the output.
- The **output current** is sampled by connecting feedback network in series with the output.



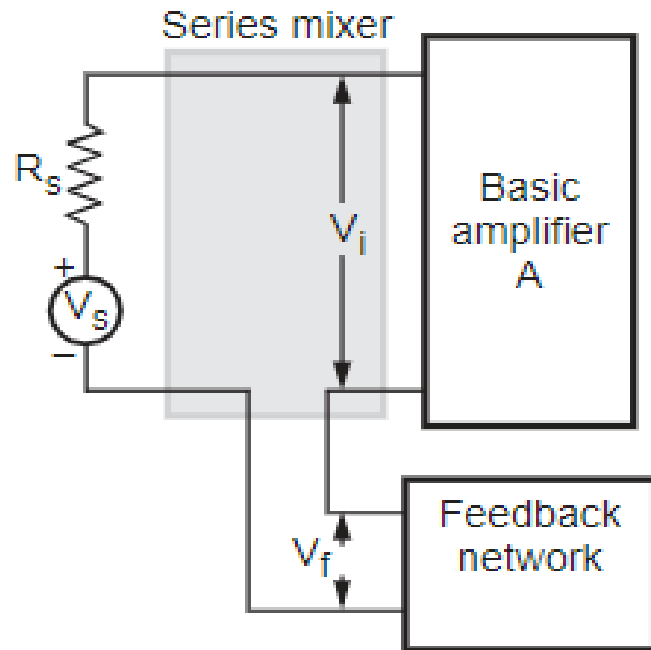
(a) Voltage or node sampling



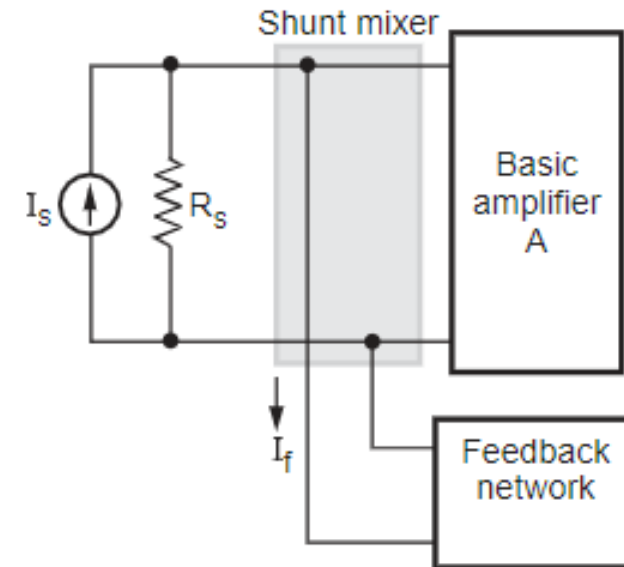
(b) Current or loop sampling

Feedback Structure

Mixer Network:



(a) Series mixing



(b) Shunt mixing

Basic Feedback Topologies

Sampling	Mixing	Topology
Voltage	Shunt	Voltage Shunt feedback
Voltage	Series	Voltage Series feedback
Current	Shunt	Current Shunt feedback
Current	Series	Current Series feedback

The Effect of Negative Feedback on Amplifier Characteristics are summarized below

Characteristics	Type of Feedback			
	Voltage Series	Voltage Shunt	Current Series	Current Shunt
Voltage Gain	Decreases	Decreases	Decreases	Decreases
Bandwidth	Increases	Increases	Increases	Increases
Harmonic distortion	Decreases	Decreases	Decreases	Decreases
Noise	Decreases	Decreases	Decreases	Decreases
Input Resistance	Increases	Decreases	Increases	Decreases
Output Resistance	Decreases	Decreases	Increases	Increases

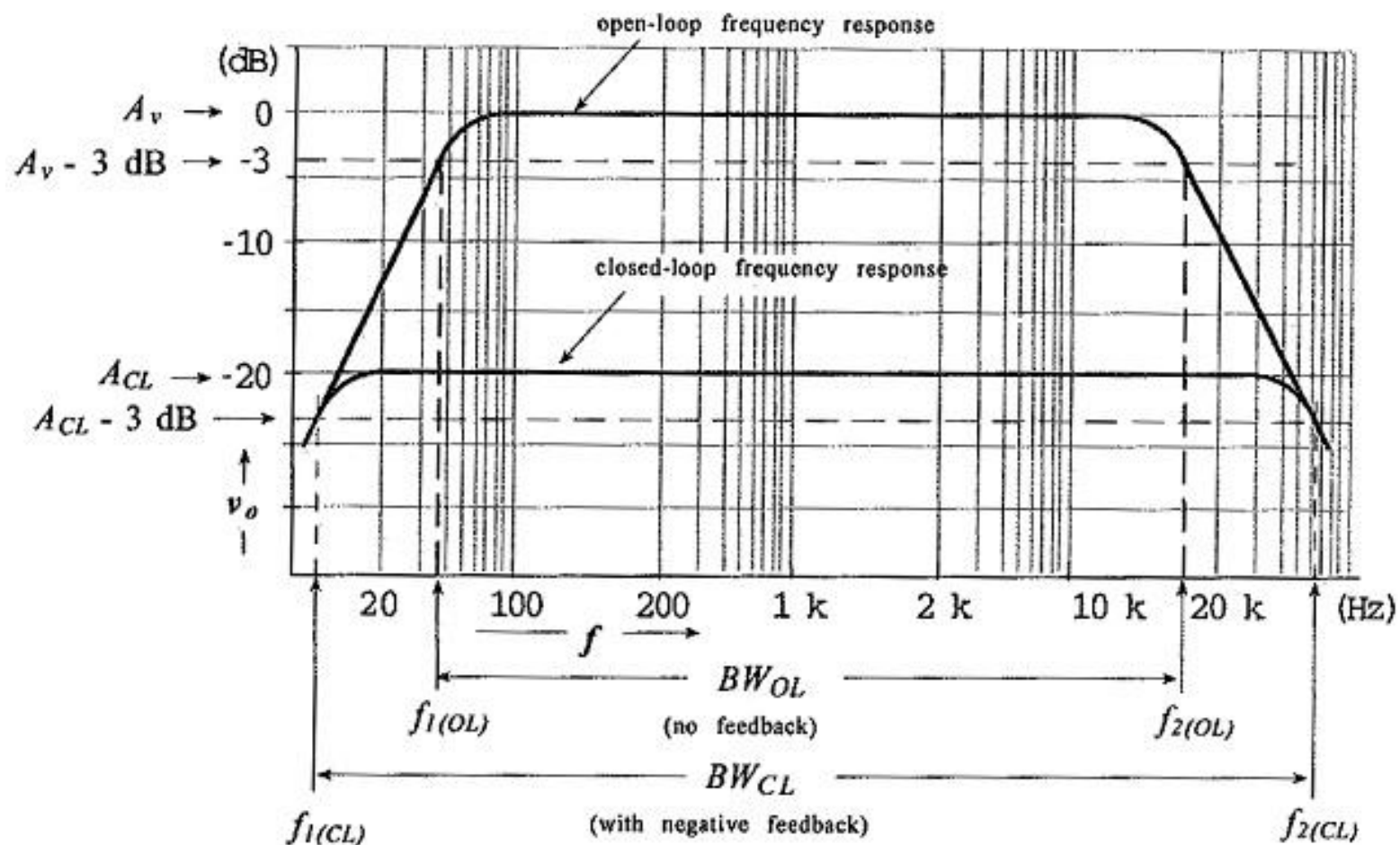
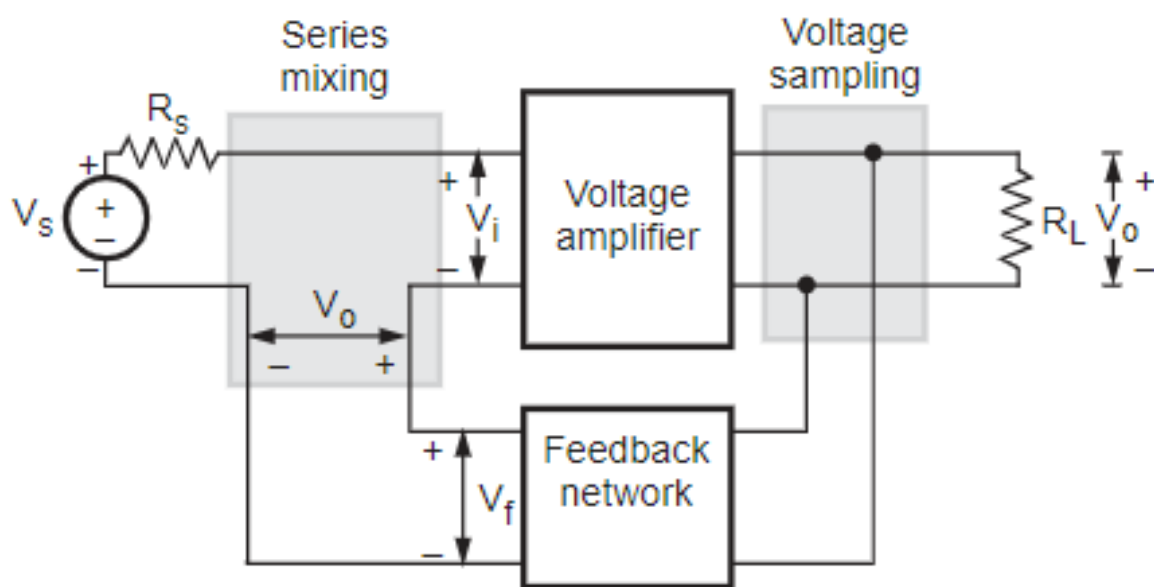


Figure 13-32

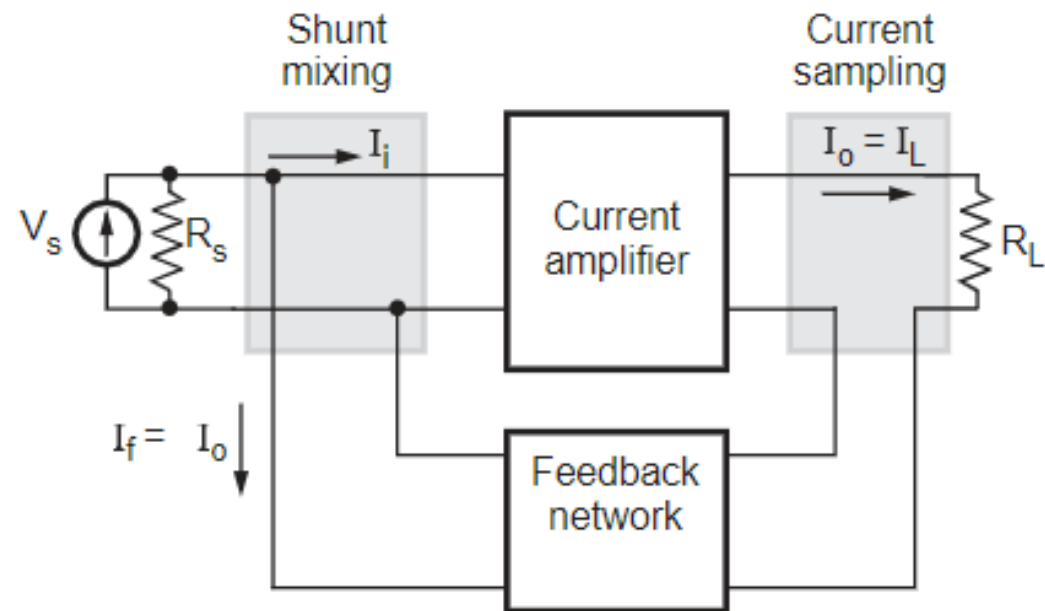
Amplifier frequency response with and without negative feedback. Negative feedback extends the amplifier bandwidth.

Basic Feedback Topologies

Sampling	Mixing	Topology
Voltage	Shunt	Voltage shunt feedback
Voltage	Series	Voltage Series feedback
Current	Shunt	Current Shunt feedback
Current	Series	Current series feedback

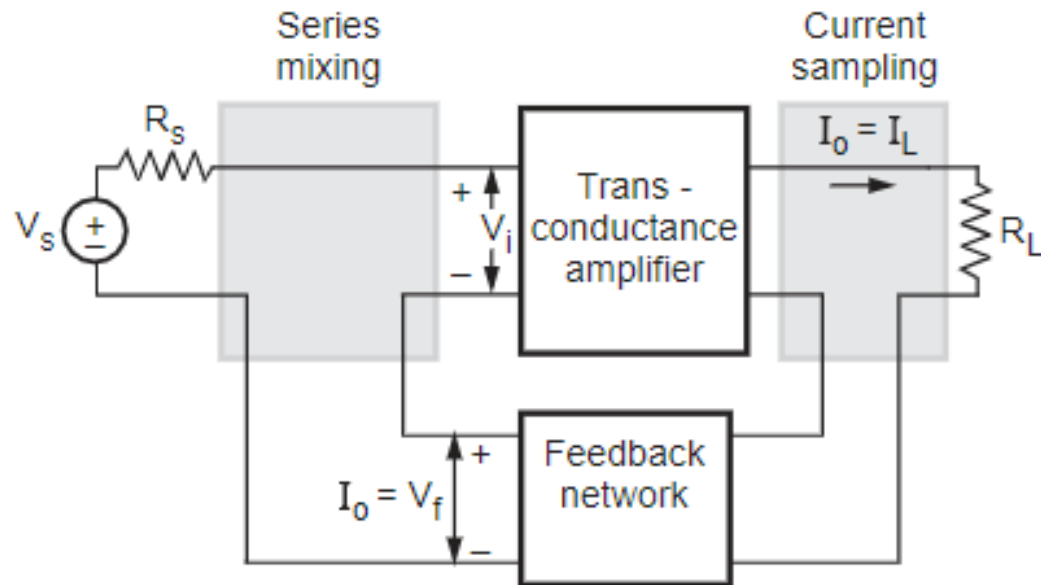


Voltage amplifier with voltage series feedback

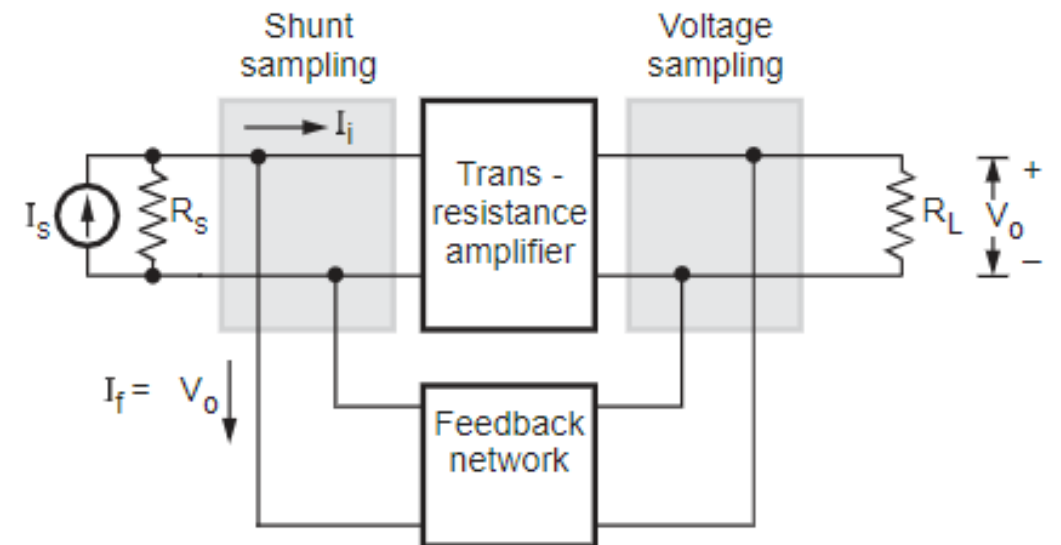


Current amplifier with current shunt feedback

Basic Feedback Topologies

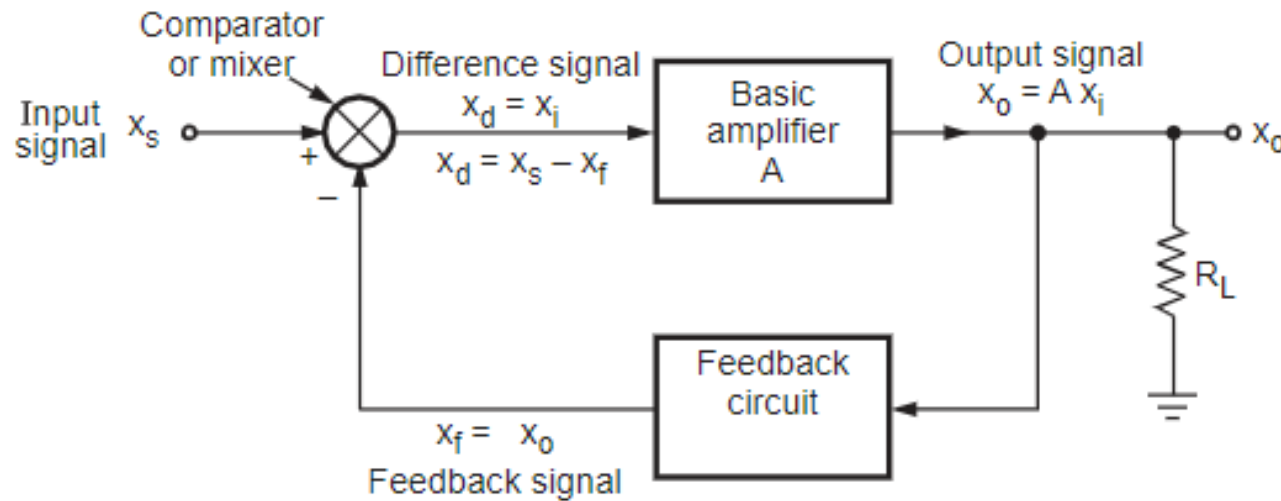


Trans-conductance amplifier with current series feedback



Trans-resistance amplifier with voltage shunt feedback

Gain with Feedback



$$A = \frac{x_o}{x_i} \quad \text{and} \quad A_f = \frac{x_o}{x_s}$$

A = Transfer gain of Basic amplifier without feedback

A_f = Transfer gain of Basic amplifier with feedback

Where,

X_O = Output voltage or output current.

X_I = Input voltage or input current.

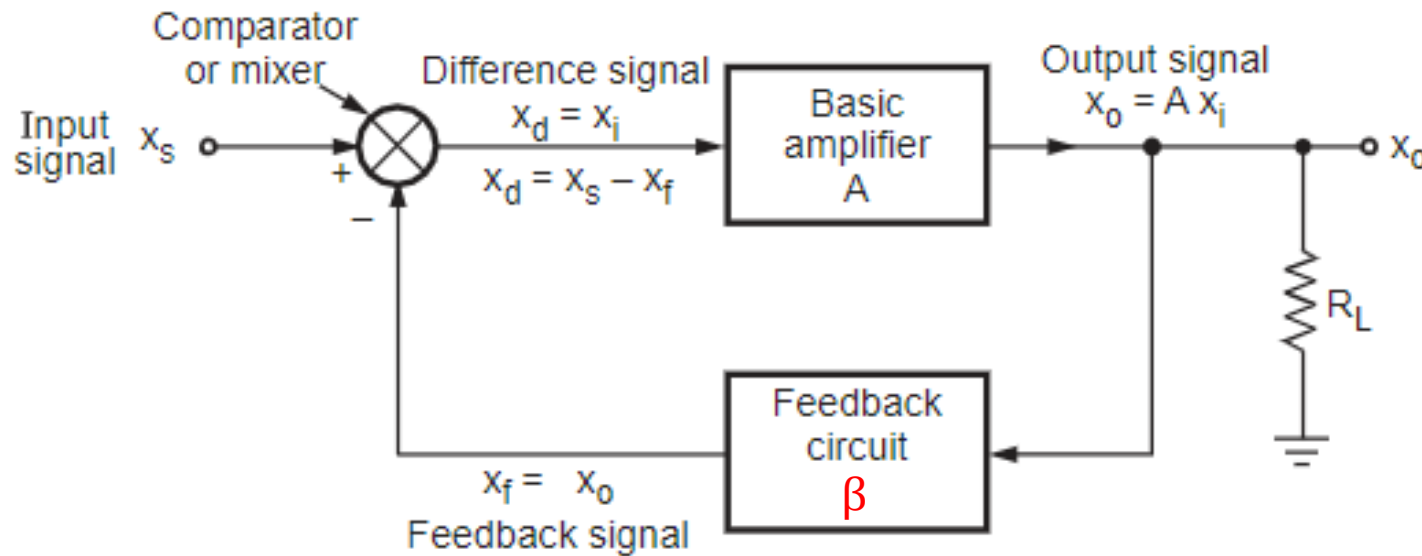
X_S = Source voltage or source current.

$$X_I = X_S - X_f$$

X_f = feedback voltage or feedback current.

$$A_f = \frac{X_o}{X_s} = \frac{X_o}{X_i + X_f}$$

Gain with Feedback



β = Feedback factor or feedback ratio lies between 0 to 1

$$A_f = \frac{X_o}{X_s} = \frac{X_o}{X_i + X_f}$$

$$A_f = \frac{X_o/X_i}{1 + X_f/X_i}$$

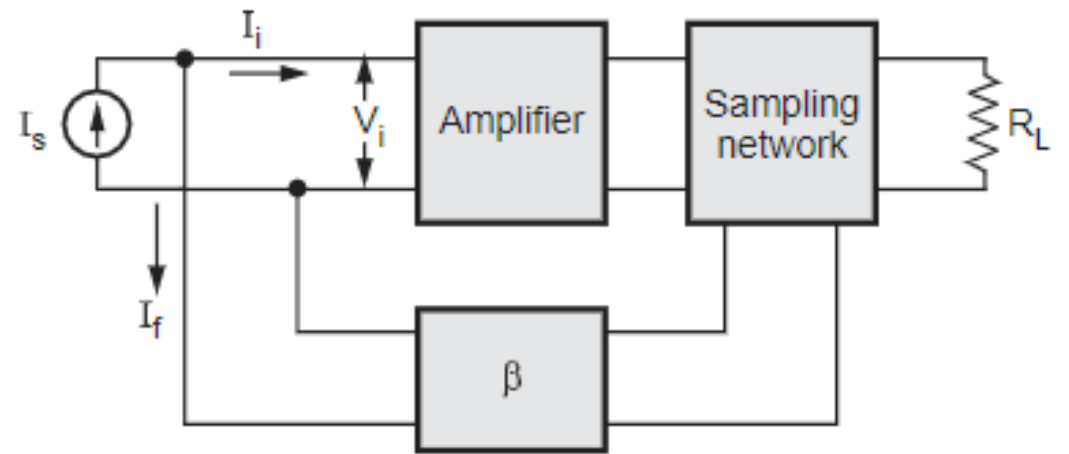
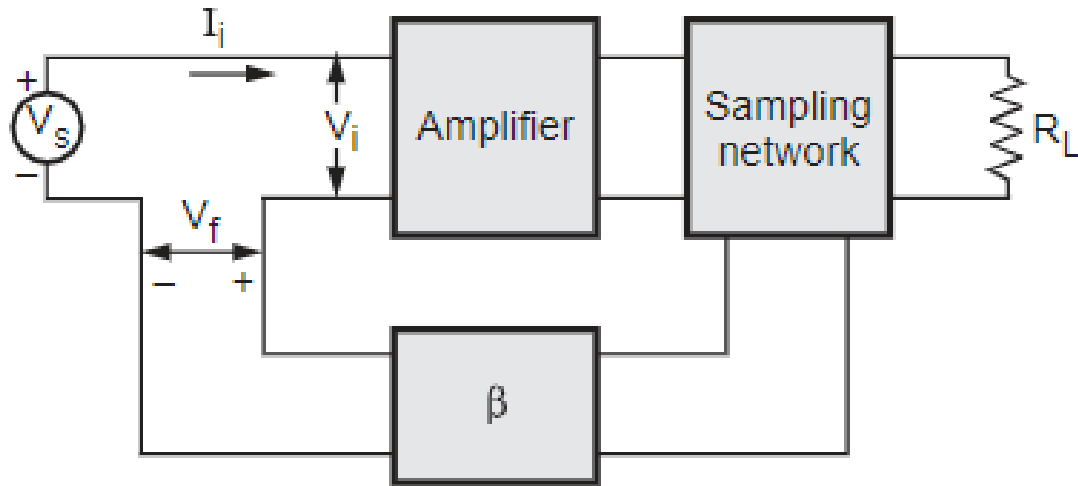
$$A_f = \frac{A}{1 + \left[\frac{X_f}{X_o} * \frac{X_o}{X_i} \right]}$$

$$A_f = \frac{A}{1 + [\beta A]}$$

Effect of Feedback on Input Resistance

Voltage Amplifier:

If feedback signal is added in series with the input signal, it increases the input resistance.
If feedback signal is added in shunt with the input signal, it decreases the input resistance.



Input resistance of Voltage Series Feedback

Input resistance with feedback:

$$R_{if} = \frac{V_S}{I_i}$$

Applying KVL to the input side we get;

$$V_S - I_i R_i - V_f = 0$$

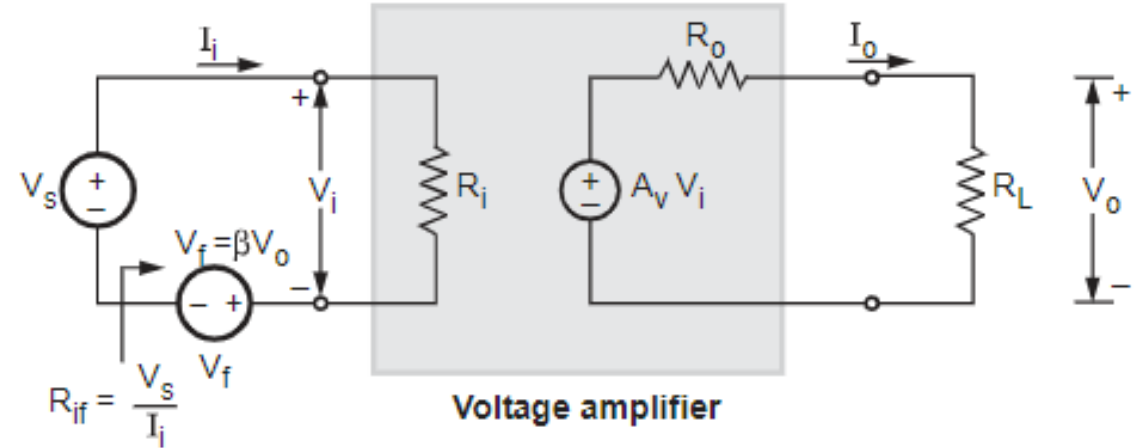
$$V_S = I_i R_i + V_f = I_i R_i + \beta V_O$$

The output voltage is given by;

$$V_O = \frac{A_v V_i R_L}{R_O + R_L} = A_V V_i$$

$$\text{Where, } A_V = \frac{A_v R_L}{R_O + R_L}$$

$$V_O = A_V I_i R_i$$



$$V_S = I_i R_i + \beta V_O = I_i R_i + \beta A_V I_i R_i$$

$$R_{if} = \frac{V_S}{I_i} = R_i + \beta A_V R_i$$

$$R_{if} = \frac{V_S}{I_i} = R_i [1 + \beta A_V]$$

Input resistance of Current Series Feedback

Input resistance with feedback:

$$R_{if} = \frac{V_S}{I_i}$$

Applying KVL to the input side we get;

$$V_S - I_i R_i - V_f = 0$$

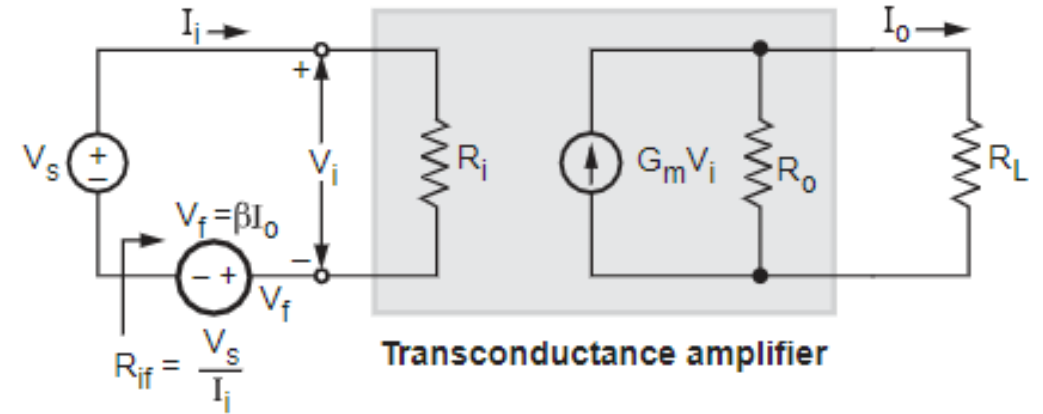
$$V_S = I_i R_i + V_f = I_i R_i + \beta I_O$$

The output current is given by;

$$I_O = \frac{G_m V_i R_O}{R_O + R_L} = G_M V_i$$

$$\text{Where, } G_M = \frac{G_m R_O}{R_O + R_L}$$

$$I_O = G_M I_i R_i$$



$$V_S = I_i R_i + \beta I_O = I_i R_i + \beta G_M I_i R_i$$

$$R_{if} = \frac{V_S}{I_i} = R_i + \beta G_M R_i$$

$$R_{if} = \frac{V_S}{I_i} = R_i [1 + \beta G_M]$$

Input resistance of Current Shunt Feedback

Input resistance with feedback:

$$R_{if} = \frac{V_I}{I_S}$$

Applying KCL to the input side we get;

$$I_S = I_i + I_f$$

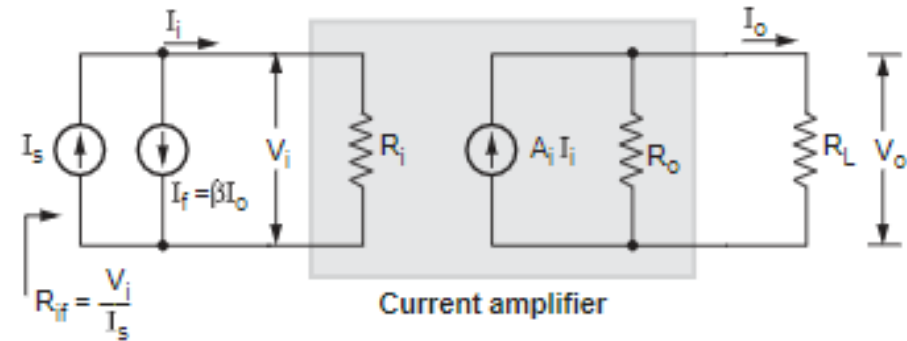
$$I_S = I_i + \beta I_O$$

The output current is given by;

$$I_O = \frac{A_i I_i R_O}{R_O + R_L} = A_I I_i$$

Where, $A_I = \frac{A_i R_O}{R_O + R_L}$

$$I_S = I_i + \beta I_O = I_i + \beta A_I I_i = I_i [1 + \beta A_I]$$



$$R_{if} = \frac{V_I}{I_S} = \frac{V_I}{I_i(1 + \beta A_I)}$$

$$R_{if} = \frac{V_I}{I_S} = \frac{R_I}{(1 + \beta A_I)}$$

Input resistance of Voltage Shunt Feedback

Input resistance with feedback:

$$R_{if} = \frac{V_I}{I_S}$$

Applying KCL to the input side we get;

$$I_S = I_i + I_f$$

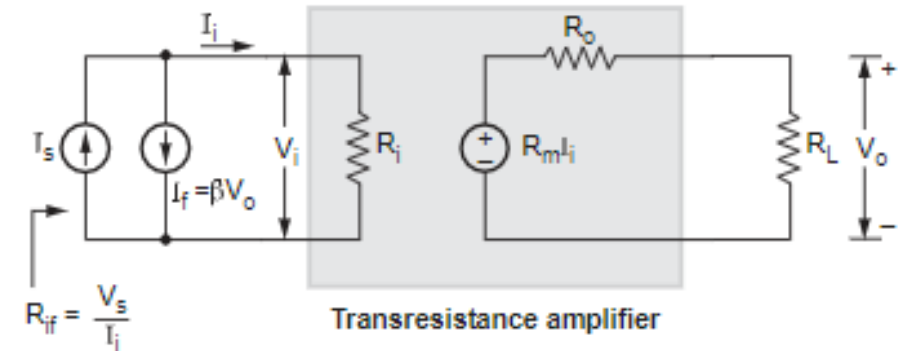
$$I_S = I_i + \beta V_O$$

The output voltage is given by;

$$V_O = \frac{R_m I_i R_O}{R_O + R_L} = R_M I_i$$

Where, $R_M = \frac{R_m R_O}{R_O + R_L}$

$$I_S = I_i + \beta I_O = I_i + \beta R_M I_i = I_i [1 + \beta R_M]$$



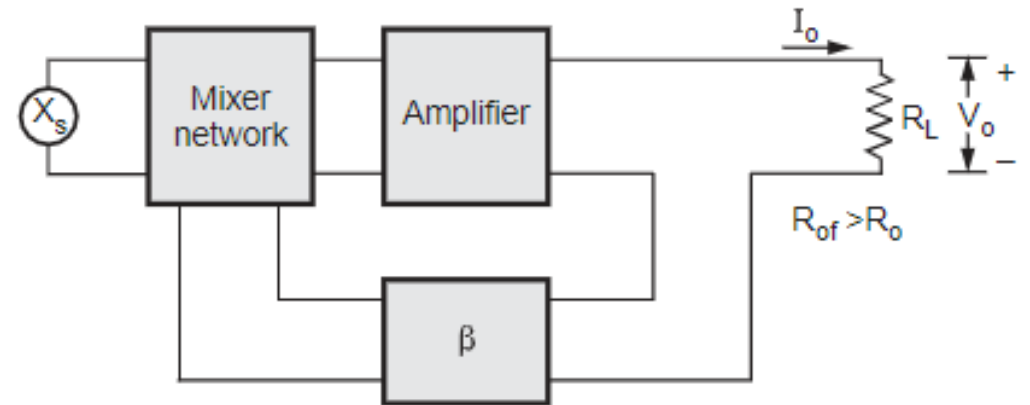
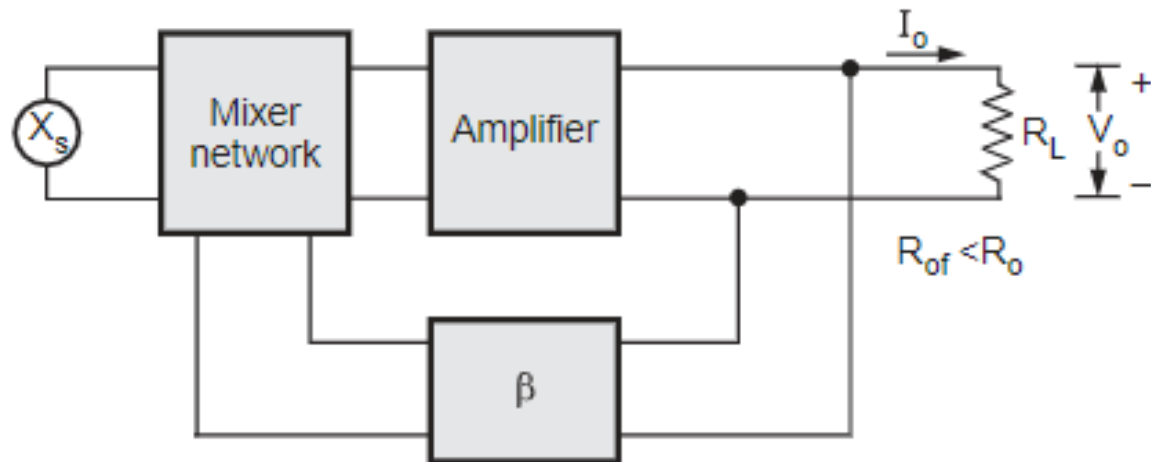
$$R_{if} = \frac{V_I}{I_S} = \frac{V_I}{I_i(1 + \beta R_M)}$$

$$R_{if} = \frac{V_I}{I_S} = \frac{R_I}{(1 + \beta R_M)}$$

Effect of Feedback on Output Resistance

The negative feedback signal which samples the output voltage, it decreases the output resistance.

The negative feedback signal which samples the output current, it increases the output resistance.



Output resistance of Voltage Series Feedback

Output resistance with feedback:

Applying KVL to the output side we get;

$$A_v V_i + IR_o - V = 0$$

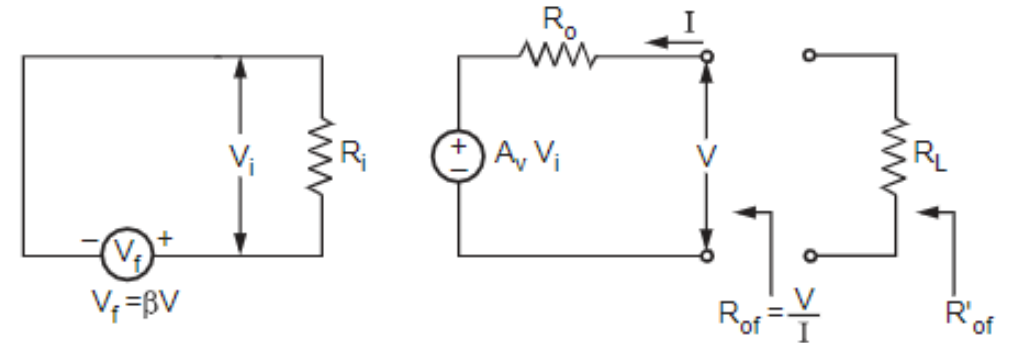
$$I = \frac{V - A_v V_i}{R_o}$$

The input voltage is given as;

$$V_i = -V_f = -\beta V$$

$$I = \frac{V + \beta A_v V}{R_o} = \frac{V(1 + \beta A_v)}{R_o}$$

$$R_{of} = \frac{V}{I} = \frac{R_o}{1 + \beta A_v}$$



$$R_{of}^1 = R_{of} \parallel R_L = \frac{R_{of} * R_L}{R_{of} + R_L}$$

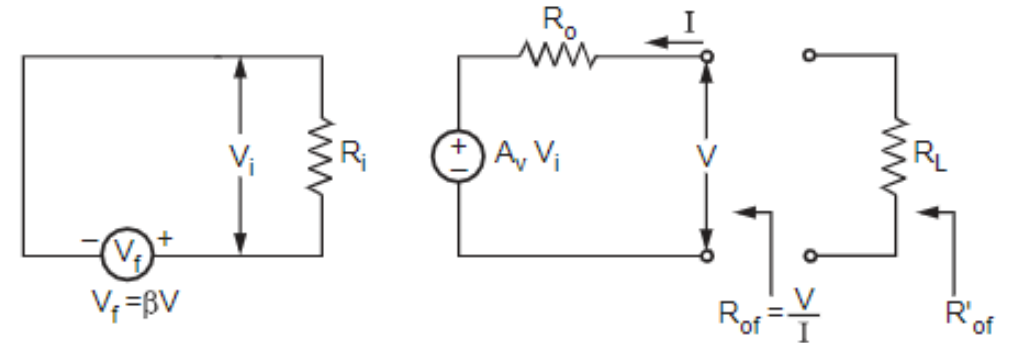
Output resistance of Voltage Series Feedback

$$R_{of}^1 = R_{of} \parallel R_L = \frac{R_{of} * R_L}{R_{of} + R_L}$$

$$\frac{\left(\frac{R_o}{1 + \beta A_v} \right) \times R_L}{\frac{R_o}{(1 + \beta A_v)} + R_L}$$

$$= \frac{R_o R_L}{R_o + R_L (1 + \beta A_v)} = \frac{R_o R_L}{R_o + R_L + \beta A_v R_L}$$

$$R'_{of} = \frac{\frac{R_o R_L}{R_o + R_L}}{1 + \frac{\beta A_v R_L}{R_o + R_L}}$$



$$R'_{of} = \frac{R'_o}{1 + \beta A_v}$$

$$\therefore R'_o = \frac{R_o R_L}{R_o + R_L} \text{ and } A_v = \frac{A_v R_L}{R_o + R_L}$$

Output resistance of Voltage Shunt Feedback

Output resistance with feedback:

Applying KVL to the output side we get;

$$R_m I_i + I R_O - V = 0$$

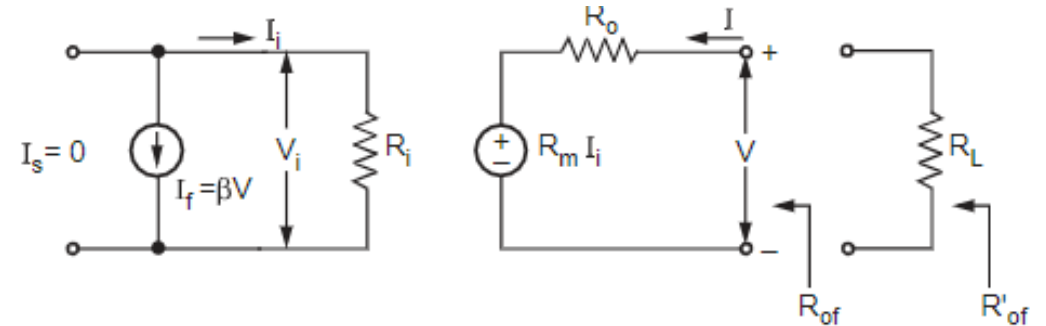
$$I = \frac{V - R_m I_i}{R_O}$$

The input current is given as;

$$I_i = -I_f = -\beta V$$

$$I = \frac{V + \beta R_m V}{R_O} = \frac{V(1 + \beta R_m)}{R_O}$$

$$R_{of} = \frac{V}{I} = \frac{R_O}{1 + \beta R_m}$$



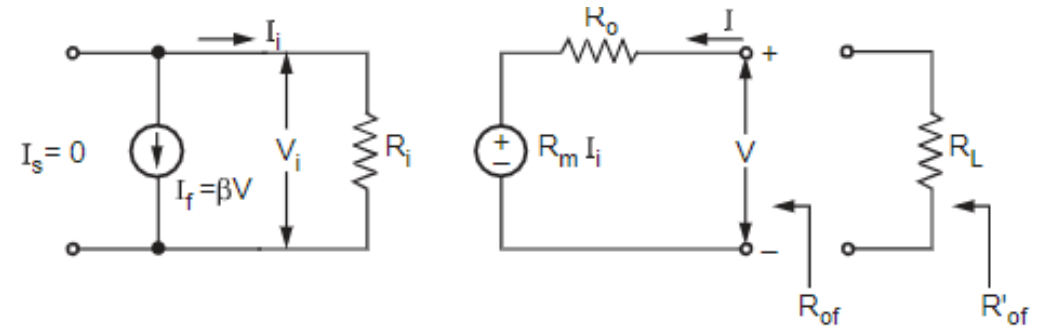
$$R_{of}^1 = R_{of} \parallel R_L = \frac{R_{of} * R_L}{R_{of} + R_L}$$

Output resistance of Voltage Shunt Feedback

$$R_{of}^1 = R_{of} \parallel R_L = \frac{R_{of} * R_L}{R_{of} + R_L}$$

$$= \frac{\frac{R_o \times R_L}{1 + R_m \beta}}{\frac{R_o}{1 + R_m \beta} + R_L} = \frac{R_o R_L}{R_o + R_L (1 + R_m \beta)}$$

$$R'_{of} = \frac{\frac{R_o R_L}{R_o + R_L}}{1 + \frac{\beta R_m R_L}{R_o + R_L}}$$



$$R'_{of} = \frac{R'_o}{1 + \beta R_M}$$

where $R'_o = \frac{R_L \times R_{of}}{R_L + R_{of}}$ and $R_M = \frac{R_m R_L}{(R_o + R_L)}$

Output resistance of Current Series Feedback

Output resistance with feedback:

Applying KCL to the output side we get;

$$I = \frac{V}{R_o} - G_m V_i$$

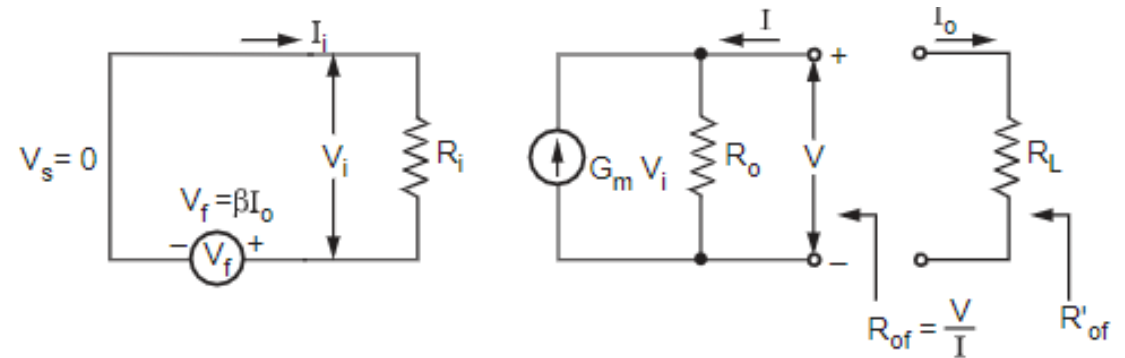
The input voltage is given as;

$$V_i = -V_f = -\beta I_o = \beta I$$

$$I = \frac{V}{R_o} - G_m \beta I$$

$$\frac{V}{R_o} = I + G_m \beta I$$

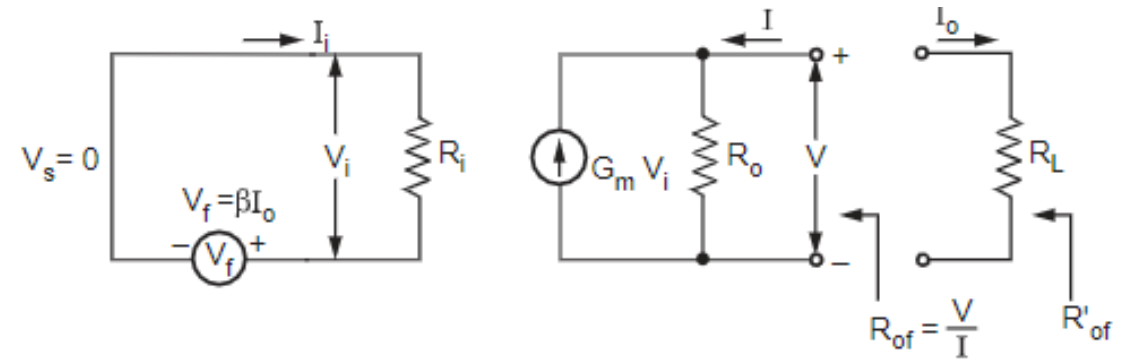
$$R_{of} = \frac{V}{I} = R_o(1 + \beta G_m)$$



$$R_{of}^1 = R_{of} \parallel R_L = \frac{R_{of} * R_L}{R_{of} + R_L}$$

Output resistance of Current Series Feedback

$$R_{of}^1 = R_{of} \parallel R_L = \frac{R_{of} * R_L}{R_{of} + R_L}$$



$$R'_{of} = R_{of} \parallel R_L = \frac{R_{of} \times R_L}{R_{of} + R_L} = \frac{R_o (1 + \beta G_m) R_L}{R_o (1 + \beta G_m) + R_L} = \frac{R_o R_L (1 + \beta G_m)}{R_o + R_L + \beta G_m R_o}$$

$$R'_{of} = \frac{R_L R_o (1 + \beta G_m)}{R_o + R_L + \frac{\beta G_m R_o}{1 + \frac{\beta G_m R_o}{R_o + R_L}}}$$

$$R'_{of} = \frac{R_o (1 + \beta G_m)}{1 + \beta G_M}$$

$$R_o' = \frac{R_o R_L}{R_o + R_L} \text{ and } G_M = \frac{G_m R_o}{R_o + R_L}$$

Output resistance of Current Shunt Feedback

Output resistance with feedback:

Applying KCL to the output side we get;

$$I = \frac{V}{R_o} - A_i I_i$$

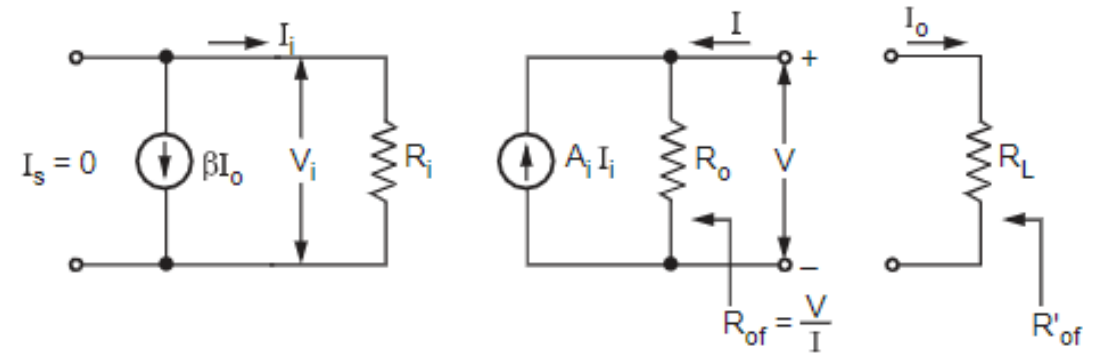
The input current is given as;

$$I_i = -I_f = -\beta I_o = \beta I$$

$$I = \frac{V}{R_o} - A_i \beta I$$

$$\frac{V}{R_o} = I + A_i \beta I$$

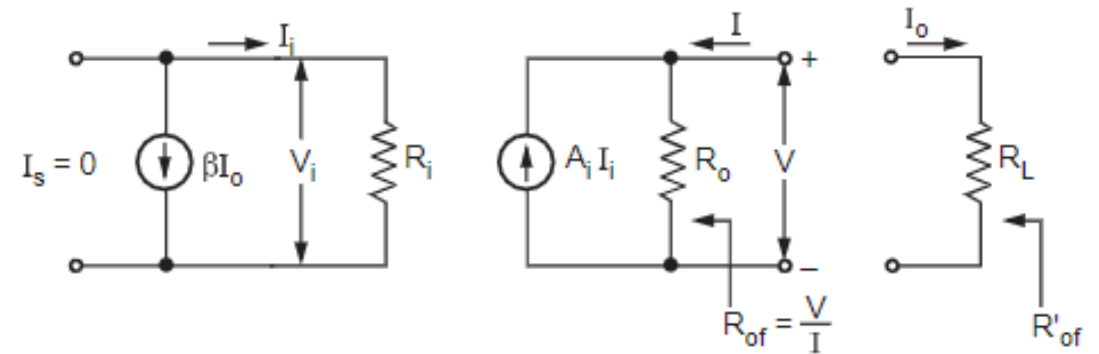
$$R_{of} = \frac{V}{I} = R_o(1 + \beta A_i)$$



$$R_{of}^1 = R_{of} \parallel R_L = \frac{R_{of} * R_L}{R_{of} + R_L}$$

Output resistance of Current Shunt Feedback

$$R_{of}^1 = R_{of} \parallel R_L = \frac{R_{of} * R_L}{R_{of} + R_L}$$



$$R'_{of} = R_{of} \parallel R_L = \frac{R_{of} \times R_L}{R_{of} + R_L} = \frac{R_o (1 + \beta A_i) R_L}{R_o (1 + \beta A_i) + R_L} = \frac{R_o R_L (1 + \beta A_i)}{R_o + R_L + \beta A_i R_o}$$

$$R'_{of} = \frac{\frac{R_o R_L (1 + \beta A_i)}{R_o + R_L}}{1 + \frac{\beta A_i R_o}{R_o + R_L}}$$

$$R'_{of} = \frac{R_o' (1 + \beta A_i)}{(1 + \beta A_i)}$$

$$R_o' = \frac{R_o R_L}{R_o + R_L} \text{ and } A_i = \frac{A_i R_o}{R_o + R_L}$$

Feedback Amplifiers

Advantages of Negative feedback:

1. **Negative feedback stabilizes transfer gain.**
2. **Reduces Non-linear distortion by a factor, $1 + \beta A$.**
3. **Noise output is reduced by a factor, $1 + \beta A$.**
4. **Negative feedback reduces frequency distortion.**
5. **Voltage amplifier generally have high input resistance and low output resistance. Negative feedback further increases the input resistance and further decreases the output resistance.**
6. **Improves frequency response of the amplifier.**

Feedback Amplifiers: Solved Examples

1. Determine the voltage gain, input and output impedance with feedback for voltage series having $A = -100$, $R_i = 10k\Omega$ and $R_o = 20k\Omega$ for feedback $\beta = -0.1$.

1. Voltage Gain with feedback

$$A_f = \frac{A}{1 + \beta A}$$

$$A_f = \frac{-100}{1 + (-0.1)(-100)} = -9.09$$

2. Input resistance with feedback

$$R_{if} = R_i (1 + \beta A_v)$$

$$R_{if} = 10k (1 + (-0.1)(-100))$$

$$R_{if} = 110 k\Omega$$

3. Output resistance with feedback

$$R_{of} = \frac{R_o}{1 + \beta A_v}$$

$$R_{of} = \frac{20k}{1 + (-0.1)(-100)} = 1.818k\Omega$$

Feedback Amplifiers: Solved Examples

2. An amplifier with negative feedback has a voltage gain of 120. It is found that without feedback an input signal of 60 mV is required to produce a particular output, whereas with feedback the input signal must be 0.5V to get the same output. Find A_v and β .

Given: $A_{vf} = 120$

$$A_v = \frac{V_o}{V_s} = \frac{V_o}{60mV}$$

$$A_{vf} = \frac{V_o}{0.5}$$

$$V_o = A_{vf} * 0.5 = 120 * 0.5 = 60V$$

$$A_v = \frac{V_o}{V_s} = \frac{V_o}{60mV} = \frac{60}{60mV} = 1000$$

$$A_{vf} = \frac{A_v}{1 + \beta A_v}$$

$$120 = \frac{1000}{1 + \beta * 1000}$$

$$\beta = 0.00733$$

Feedback Amplifiers: Solved Examples

3. An amplifier has a voltage gain of 4000. Its input impedance is 2k Ω and output impedance is 60k Ω . Calculate the voltage gain, input and output impedance of the circuit if 5% of the feedback is fed in the form of series negative voltage feedback.

1. Voltage Gain with feedback

$$A_f = \frac{A}{1 + \beta A}$$

$$A_f = \frac{4000}{1 + (0.05)(4000)} = 19.9$$

2. Input resistance with feedback

$$R_{if} = R_i (1 + \beta A_v)$$

$$R_{if} = 2k (1 + (0.05)(4000))$$

$$R_{if} = 402 \text{ k}\Omega$$

3. Output resistance with feedback

$$R_{of} = \frac{R_o}{1 + \beta A_v}$$

$$R_{of} = \frac{60k}{1 + (0.05)(4000)} = 298.5\Omega$$

THANK YOU